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## Masonry Walls

Lab Recitation \#11
Group \#3

April 12020

University of Michigan, TCAUP

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## 11. Masonry Walls

Using the strength method for axial compression described in TMS 402, determine the safety of the given concrete masonry wall (pass or fail). Calculate the factored nominal axial strength, phi_Pn and compare it to the required strength, Pu for the given loads. (loads are given without factors)

## DATASET: 1 -2- $-3-$

| Height of wall, h | 21 FT |
| :--- | ---: |
| Nominal thickness of wall | 16 IN |
| grouted cells o.c. spacing | 40 IN |
| Masonry compressive strength, fm | 1500 PSI |
| The wall DL | 17 KLF |
| The wall LL | 13 KLF |

## Q\#1 Actual wall thickness, t

$$
\begin{aligned}
& T=16 "-3 / 8^{\prime \prime}=15 \text { 5/8" } \\
& \text { (given) (common) }
\end{aligned}
$$

DATASET: 1
Heinht of wall
$\mathrm{h}^{-2-}$
-3-

| Nominal thickness of wall | 16 IN |
| :--- | ---: |
| grourea cels o.c. spacing | 40 IN |
| Masonry compressive strength, fm | 1500 PSI |
| The wall DL. | 17 KLF |
| The wall LL. | 13 KLF |



## Q\#2 Net area per foot of wall, $\mathrm{A}_{\mathrm{n}}$

Find $A_{n}$ at Tek 14-1B table (available in canvas)

| An at Tek 14-1B table (available in |  |  |  |  |  | al thicknes <br> d cells o.c | ss of wall spacing |  | $\begin{aligned} & 16 \mathrm{IN} \\ & 40 \mathrm{IN} \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\rangle$ |  |  |  |  | all DL all LL |  |  | $\begin{aligned} & 17 \mathrm{KL} \\ & 13 \mathrm{KL} \end{aligned}$ |  |
| $A n=63$ |  |  |  |  |  |  |  |  |  |  |
|  |  | Table 7- | inch (406- | m) ) ingle | ythe | 1/4 in. (32 | mm ) Face | Shells (stan | dard) |  |
|  |  |  | 7a: Horizon | al Section | Properties | Masonry Sp | anning Ver | tically) |  |  |
|  |  | Grout | Mortar | Net cros | -sectional | operties^ | Avera | ge cross-sect | tional proper | ies ${ }^{\text {B }}$ |
|  | Unit | spacing (in.) | bedding | $A_{n}\left(\mathrm{in} .^{2} \mathrm{ff}\right)$ | $I_{n}(\mathrm{in} .4 / \mathrm{ft})$ | $S_{n}\left(\mathrm{in} .{ }^{3} / \mathrm{ft}\right)$ | $A_{\text {anz }}\left(\mathrm{in.}^{2} / \mathrm{ft}\right)$ | $I_{\text {avz }}$ (in. ${ }^{4} \mathrm{ft}$ ) | $S_{\text {avz }}\left(\mathrm{in} .^{3} / \mathrm{ft}\right)$ | $r_{\text {ang }}$ (in.) |
|  | Hollow | No grout | Face shell | 30.0 | 1,553.7 | 198.9 | 63.2 | 2,030.6 | 259.9 | 5.67 |
|  | Hollow | No grout | Full | 63.2 | 2,030.6 | 259.9 | 63.2 | 2,030.6 | 259.9 | 5.67 |
|  | 100\% so | id/solidly grouted | Full | 187.5 | 3,814.7 | 488.3 | 187.5 | 3,814.7 | 488.3 | 4.51 |
|  | Hollow | 16 | Face shell | 112.4 | 2,737.2 | 350.4 | 123.5 | 2,896.2 | 370.7 | 4.84 |
|  | Hollow | $24$ | Face shell | $85.0$ | 2,342.7 | $299.9$ | 103.4 | 2,607.7 | 333.8 | 5.02 |
|  | Hollow | $32$ | Eace shell | 71.2 | 2.145 .5 | 274.6 | 93.4 | 2,463.4 | 315.3 | 5.14 |
| Look for 40" grout spacing | Hollow | 40 | Face shell | 63.0 | 2,027.1 | 259.5 | 87.3 | 2,376.9 | 304.2 | 5.22 |
| Look for 40 grout spacing |  | +0 | тatesmı | 97. | +,40.2 | 249.4 | 83.3 | 2,319.1 | 296.9 | 5.28 |
|  | Hollow | 72 | Face shell | 48.3 | 1,816.7 | 232.5 | 76.6 | 2,223.0 | 284.5 | 5.39 |
|  | Hollow | 96 | Face shell | 43.7 | 1,751.0 | 224.1 | 73.3 | 2,174.9 | 278.4 | 5.45 |
|  | Hollow | 120 | Face shell | 41.0 | 1,711.5 | 219.1 | 71.3 | 2,146.0 | 274.7 | 5.49 |

## Q\#3 Net moment of inertia per foot of wall, $\mathrm{In}_{n}$

Find moment of inertia, In at Tek 14-1B table (available in canvas)

DATASET: 1
Heinht of wall $h$ $-2$ -3-
Heimht of wall $n$
Nominal thickness of wall
grouted cells o.c. spacing

The wall DL
17 KLF
The wall LL
13 KLF
In = 2027.1


## Q\#4 Find radius of gyration per foot of wall

$$
\begin{aligned}
r & =\underset{(\text { Ans3) (Anns) }}{\sqrt{I / A}} \\
& =\sqrt{2027.1 / 63} \\
& =5.6724
\end{aligned}
$$

## DATASET: 1



## Q\#5 Ratio of h/r

$\mathrm{h} / \mathrm{r}$
$=(21 \times 12) / 5.6724$


## Q\#6 Which tms equation is used, 11 or 12

$$
h / r=44.425
$$

(Ans 5)
$=44.425<99$
Hence use equation 3-11
(a) For members having an $h / r$ ratio not greater than 99:

$$
P_{n}=0.80\left\{0.80 A_{n} f_{m}^{\prime}\left[1-\left(\frac{h}{140 r}\right)^{2}\right]\right\}(\text { Equation 3-11) }
$$

(b) For members having an $h / r$ ratio greater than 99

$$
P_{n}=0.80\left[0.80 A_{n} f_{m}^{\prime}\left(\frac{70 r}{h}\right)^{2}\right]
$$

## (Equation 3-12)

(find these equations at TMS 402, available in canvas)


## Q\#7 Nominal axial strength, Pn



## Q\#8 Factored nominal axial strength, Phi_Pn

## Phi_Pn $=0.9 \times$ Pn

(Ans 7)
(Phi for axial force is 0.9 )
$=0.9 \times 54.39$
$=48.95$

```
DATASET: 1
```

Height of wall, $h$
Nominal thickness of wall
16 IN Ninutad ralle ar anarina


## Q\#9 Required axial strength, Pu

$$
\begin{aligned}
P_{u} & =1.2(\mathrm{DL})+1.6(\mathrm{LL}) \\
& =1.2(17)+1.6(13) \\
& =41.2
\end{aligned}
$$

## DATASET: 1

Height of wall, $h$
Nominal thickness of wall
grouted cells o.c. spacing


## Q\#10 Does the wall pass or fail?

| If $\mathrm{Pu}>\mathrm{phi} \mathrm{P}_{\mathrm{n}}$ | - Fail |
| :---: | :---: |
| If $\mathrm{Pu}<\mathrm{phi} \mathrm{P}_{\mathrm{n}}$ | - Pass |
| 41.2 < | 49.95 |
| (Pu, Ans 9) | (phi Pn, Ans 8) |
| = Pass |  |

## DATASET: 1

Height of wall, $h$
Nominal thickness of wall
grouted cells o.c. spacing
16 IN


## Any Questions?

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