

Recitation



10. Composite Sections

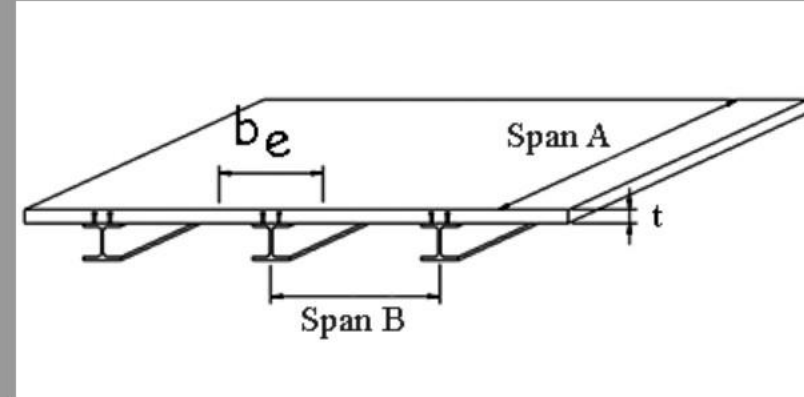
Using the strength method, determine the required amount of flexural steel reinforcement, A_s , for the simple span beam (shown in section). The beam carries a dead and live floor load from a one-way slab in addition to its own self weight at 150 PCF. For the given bar size, determine the number of bars to obtain the required A_s . Check $A_{s,min}$ and $\epsilon_{t,t}$. Calculate the strength moment, M_n for the final beam design and check that ϕM_n is $> M_u$.

DATASET: 1

-2-

-3-

W-section	W16X77
span A	49 FT
span B	11 FT
slab thickness, t	6 IN
steel yield stress, F_y	50 KSI
concrete ultimate stress, f'_c	3 KSI



#	Question	Your Response	Correct Answer
1	Effective width of the concrete flange, b_e	IN	SUBMIT
2	Depth of concrete stress block, a	IN	SUBMIT
3	Is depth a within the slab? 1=yes, 0=no		SUBMIT
4	The nominal bending moment, M_n	K-IN	SUBMIT
5	The factored bending resistance, ϕM_n	K-IN	SUBMIT
6	The factored design moment, M_u	K-FT	SUBMIT
7	The total factored design load, w_u	KLF	SUBMIT
8	The selfweight of the concrete slab	PSF	SUBMIT
9	The total (steel+concrete) unfactored dead load on the beam, w_{DL}	KLF	SUBMIT
10	The actual, unfactored beam live load (capacity), w_{LL}	KLF	SUBMIT
11	The actual floor live load (floor capacity), LL	PSF	SUBMIT

effective width

$$\min \left[\begin{array}{l} \frac{1}{4} (\text{Span of steel beam}) = \frac{1}{4} (49 \times 12) = 147 \\ b_f + 2(8 \times \text{slab thickness}) = 10 + 2(8 \times 6) = \underline{106} \checkmark \\ b_f + 2\left(\frac{1}{2} \text{ clear distance} \right) = 10 + 2\left(\frac{1}{2} (11 \times 12)\right) = 142 \\ \text{Span B} \end{array} \right]$$

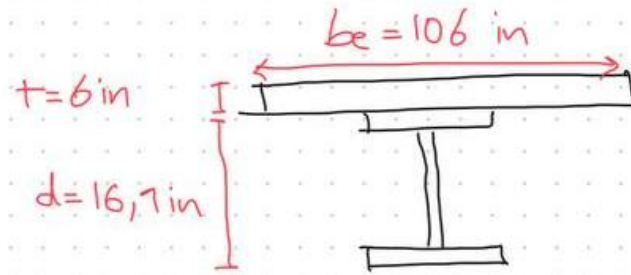
$$W 16 \times 77 \xrightarrow[\text{Table}]{\text{Based on}} \begin{array}{ll} d: 16.7 \text{ in} & b_f: 10 \text{ in} \\ A: 22.6 \text{ in}^2 & w: 77 \text{ lb/ft} \end{array}$$

effective depth of
Concrete Stress block (a)

$$a = \frac{As f_y}{0.85 f'_c b_e}$$

$$= \frac{22.6(50)}{0.85(3)(106)} = \frac{1130}{270.3} = 4.1805 < 6 \text{ in} \quad \text{Assumption is True} \checkmark$$

within slab



a is within concrete $\rightarrow$ The full steel section is in tension

Nominal bending moment = plastic moment

$$M_n = M_p = As f_y \left(\frac{d}{2} + t - \frac{a}{2} \right) = 22.6(50) \left(\frac{16.1}{2} + 6 - \frac{4.1805}{2} \right)$$
$$= 13514.18 \text{ k-in}$$

$$\phi M_n = 0.9 (13514,8) = 12163,32$$

$$M_u \leq \phi M_n \rightarrow M_u = \phi M_n = 12163,32 \times \frac{1}{12} = 1013,61 \text{ k-ft}$$

↓

ultimate moment that
section withstand

$$M_u = \frac{w_u l^2}{8} \rightarrow w_u = \frac{8 M_u}{\underset{\text{Span A}}{l^2}} = \frac{8 (1013,61)}{(49)^2} = 3,377 \text{ klf}$$

Self weight of concrete slab

$$1 \text{ ft}^2$$

$$150 \text{ lb}$$

$$\frac{6}{12}$$

$$\frac{6}{12} \times 150 = 75$$

Total unfactored dead load:

Self weight (concrete + steel)

$$(17) 75 + 77 = 902 \text{ plf} \xrightarrow{\div 1000} 0.902 \text{ klf}$$

↓
Span B

Actual unfactored live load

$$w_u = 1.2 w_D + 1.6 w_L$$

$$3,377 = 1.2 (0.902) + 1.6 w_L \rightarrow w_L = 1,434 \text{ klf}$$

Actual floor live load

$$\frac{w_L}{\text{Span}} = \frac{1,434}{18} = 0.079673 \text{ ksf} \times 1000 = 79,67 \text{ psf}$$

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- Thanks for your attention 😊