

# Arch324

# **STRUCTURES II**

Winter 2025  
Recitation

FACULTY: Prof. Peter von Bülow  
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# Arch324: STRUCTURES II

## Welcome to Recitation session 02/14

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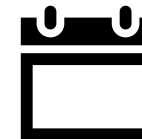
hours:

Fri: 11:30 – 12:30

Mon, Wed: 11:00 - 12:00

walk-ins welcome!

Please feel free to ask questions.



[Click here to make an appointment](#)

Where can you find me?



# Arch324: STRUCTURES II

## Welcome to Recitation session 02/14

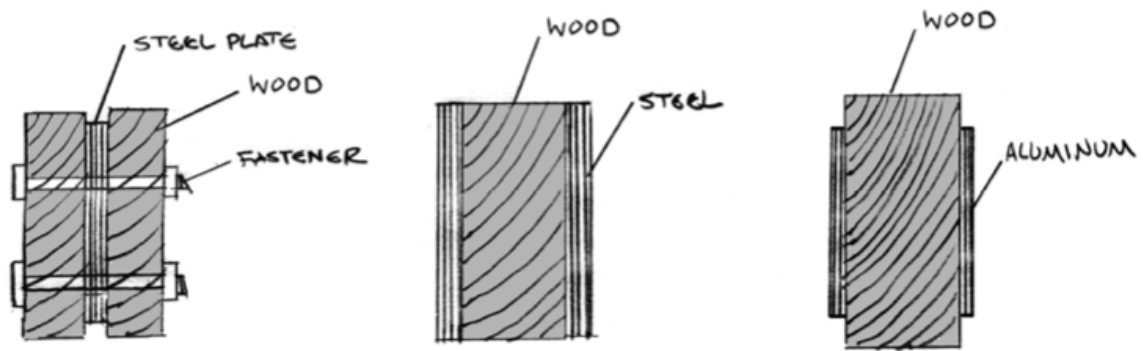
### Outline:

- Quick **Recap** of the week
- Provide the solution for the assignment (**Homework 4**)
- Answering student's questions
- Lab: **Steel beam**
- **Tower Project:** due date is extended! Feb 16

Please feel free to ask questions.

# Recap of the week

## Flitched Beams & Scab Plates





# Recap of the week

## Procedure - Analysis of Steel Beams – for Zone 1 $L_b < L_p$

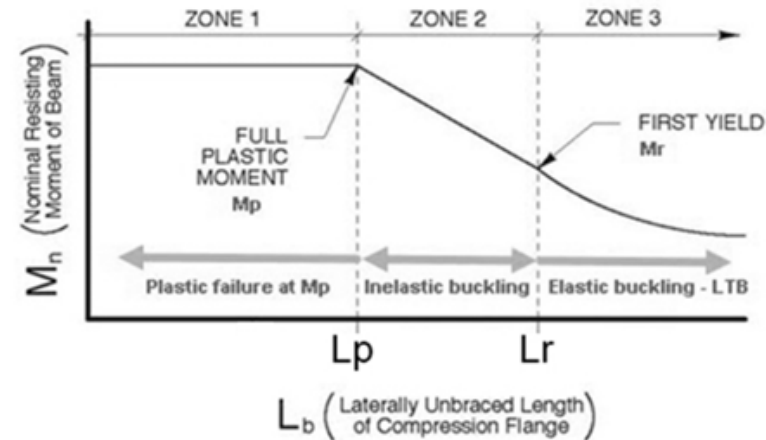
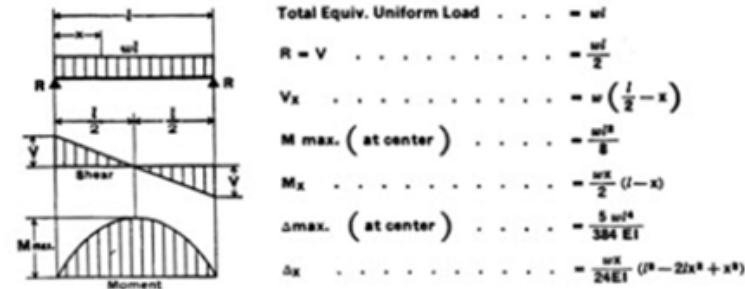
### Pass/Fail

Given: yield stress, steel section, loading, bracing ( $L_b$ )

Find: pass/fail of section

1. Calculate the factored design load  $w_u$   
 $w_u = 1.2w_{DL} + 1.6w_{LL}$
2. Determine the design moment  $M_u$ .  
 $M_u$  will be the maximum beam moment using the factored loads
3. Insure that  $L_b < L_p$  (zone 1)  
 $L_p = 1.76 r_y \sqrt{E/F_y}$
4. Determine the nominal moment,  $M_n$   
 $M_n = F_y Z_x$  (look up  $Z_x$  for section)
5. Factor the nominal moment  
 $\phi M_n = 0.90 M_n$
6. Check that  $M_u < \phi M_n$
7. Check shear
8. Check deflection

### 1. SIMPLE BEAM—UNIFORMLY DISTRIBUTED LOAD



# Recap of the week

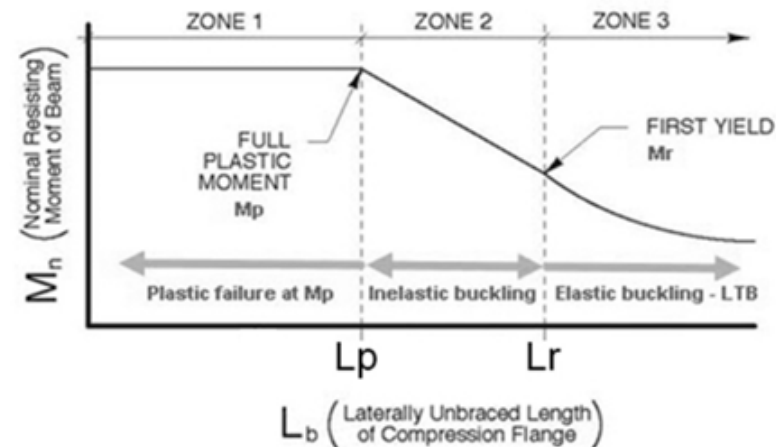
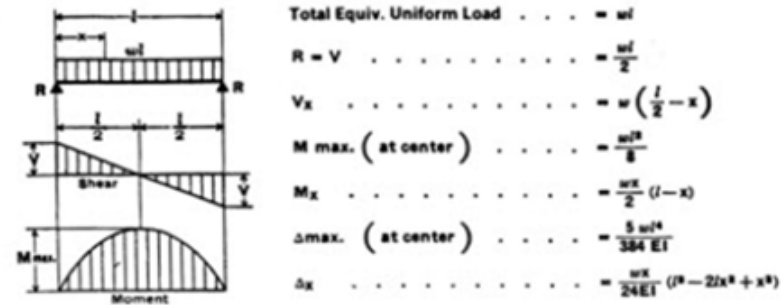
## Procedure - Analysis of Steel Beam - Capacity

Given: yield stress, steel section, bracing

Find: moment or load capacity

1. Determine the unbraced length of the compression flange ( $L_b$ ).
2. Find the  $L_p$  and  $L_r$  values from the AISC  $Z_x$  Table 3-2
3. Compare  $L_b$  to  $L_p$  and  $L_r$  and determine which equation for  $M_n$  or  $M_{cr}$  to be used.
4. Determine the beam load equation for maximum moment in the beam.
5. Calculate load based on maximum moment.  $M_u = \phi_b M_n$

### 1. SIMPLE BEAM—UNIFORMLY DISTRIBUTED LOAD



# Recap of the week

## Design of Steel Beam –Procedure (zone 1)

1. Use the maximum moment equation, and solve for the ultimate moment,  $M_u$ .
2. Set  $\phi M_n = M_u$  and solve for  $M_n$
3. Assume Zone 1 to determine  $Z_x$  required
4. Select the lightest beam with a  $Z_x$  greater than the  $Z_x$  required from AISC table
5. Determine if  $h/t_w < 59$   
(case 1, most common)
6. Determine  $A_w$ :  
 $A_w = d t_w$
7. Calculate  $V_n$ :  
 $V_n = 0.6 F_y A_w$
8. Calculate  $V_u$  for the given loading  
 $V_u = w_u L / 2$  (e.g. unif. load)
9. Check  $V_u < \phi V_n$   
 $\phi$  for  $V = 1.0$
10. Check deflection



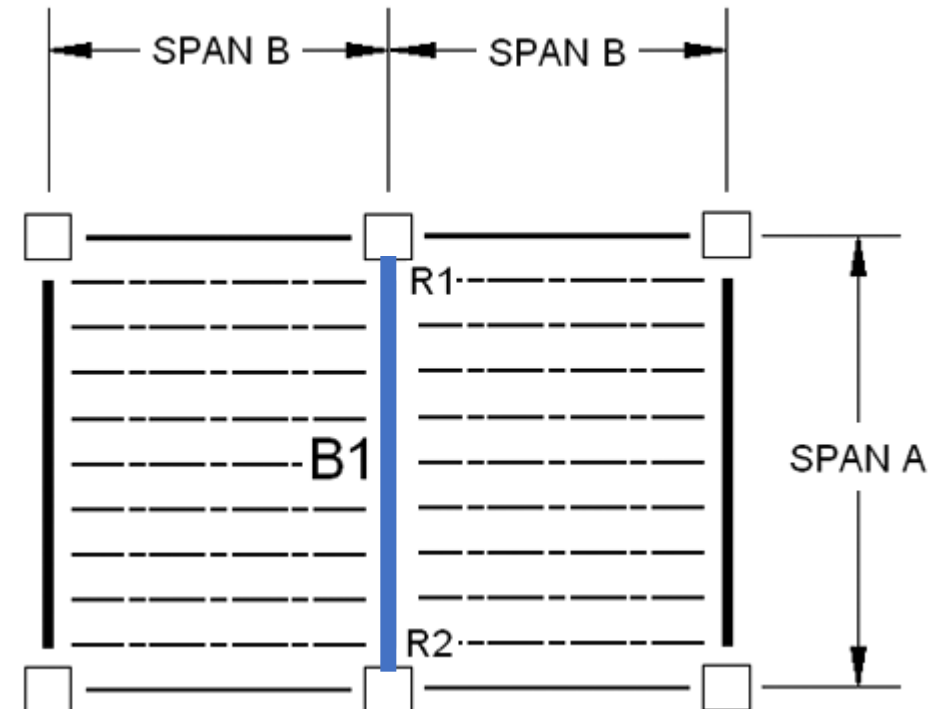
# Provide the solution for the assignment – HW4

- Problem:

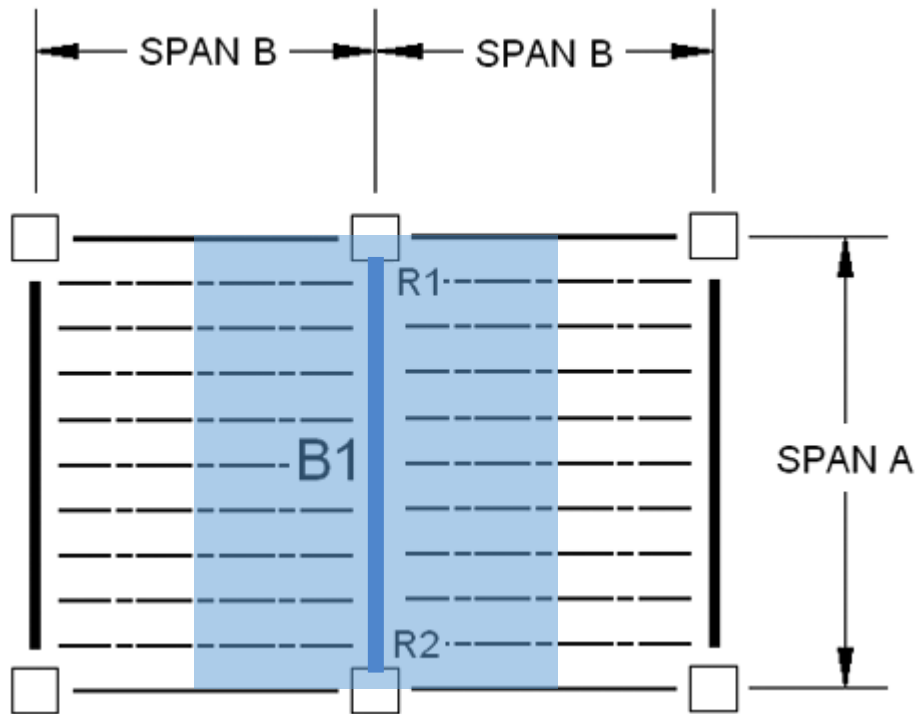
## 4. Steel Beam Analysis

Analyze the **given W-section** for beam B1, to determine the **maximum live load** capacity the floor can carry. Determine the shear and bending forces and check the maximum deflection against an allowable of  **$L/180$** . Assume the beam is fully braced,  $L_b < L_p$  (zone 1).

DATASET: 1	-2-	-3-
W-section	W12X19	
Fy	50 KSI	
Span A	21 FT	
Span B	14 FT	
Floor DL	10 PSF	



# Provide the solution for the assignment – HW3



#	Question	Your Response
1	The plastic modulus of the section, $Z_x$	<input type="text"/> IN3
2	The nominal bending moment, $M_n$	<input type="text"/> K-IN
3	The factored bending resistance, $\phi M_n$	<input type="text"/> K-IN
4	The factored design moment, $M_u$	<input type="text"/> K-FT
5	The total factored design load, $w_u$	<input type="text"/> KLF
6	The total unfactored dead load on the beam, $w_{DL}$	<input type="text"/> KLF
7	The total factored dead load on the beam, $w_{u,DL}$	<input type="text"/> KLF
8	The factored live load on the beam, $w_{u,LL}$	<input type="text"/> KLF
9	The actual beam live load (capacity), $w_{LL}$	<input type="text"/> KLF
10	The actual floor live load (floor capacity), $LL$	<input type="text"/> PSF
11	The maximum factored design beam shear force, $V_{u,max}$	<input type="text"/> K
12	The web area, $A_w$	<input type="text"/> IN2
13	The factored shear resistance, $\phi V_n$	<input type="text"/> K
14	Is the section safe for shear? (1=yes, 0=no)	<input type="text"/>
15	The actual (unfactored) deflection due to total DL + LL	<input type="text"/> IN
16	The deflection limit $L/180$	<input type="text"/> IN
17	Is the actual deflection less than the limit $L/180$ ? (1=yes, 0=no)	<input type="text"/>

# Provide the solution for the assignment – HW4

Given W-section : W12x19

→ AISC , Table 1-1

1-26


DIMENSIONS AND PROPERTIES

Table 1-1 (continued)  
W-Shapes  
Dimensions

Shape	Area, A	Depth, d	Web			Flange			Distance						Work- able Gage
			Thickness, t <sub>w</sub>	t <sub>w</sub> 2	Width, b <sub>f</sub>	Thickness, t <sub>f</sub>	k		k <sub>1</sub>	T					
							k <sub>des</sub>	k <sub>det</sub>							
	in. <sup>2</sup>	in.	in.	in.	in.	in.	in.	in.	in.	in.	in.	in.	in.		
W12×58	17.0	12.2	12 <sup>1</sup> / <sub>4</sub>	0.360	3/8	3/16	10.0	10	0.640	5/8	1.24	1 <sup>1</sup> / <sub>2</sub>	15/16	9 <sup>1</sup> / <sub>4</sub>	5 <sup>1</sup> / <sub>2</sub>
×53	15.6	12.1	12	0.345	3/8	3/16	10.0	10	0.575	9/16	1.18	1 <sup>3</sup> / <sub>8</sub>	15/16	9 <sup>1</sup> / <sub>4</sub>	5 <sup>1</sup> / <sub>2</sub>
W12×50	14.6	12.2	12 <sup>1</sup> / <sub>4</sub>	0.370	3/8	3/16	8.08	8 <sup>1</sup> / <sub>8</sub>	0.640	5/8	1.14	1 <sup>1</sup> / <sub>2</sub>	15/16	9 <sup>1</sup> / <sub>4</sub>	5 <sup>1</sup> / <sub>2</sub>
×45	13.1	12.1	12	0.335	5/16	3/16	8.05	8	0.575	9/16	1.08	1 <sup>3</sup> / <sub>8</sub>	15/16	↓	↓
×40	11.7	11.9	12	0.295	5/16	3/16	8.01	8	0.515	1/2	1.02	1 <sup>3</sup> / <sub>8</sub>	7/8	↓	↓
W12×35 <sup>c</sup>	10.3	12.5	12 <sup>1</sup> / <sub>2</sub>	0.300	5/16	3/16	6.56	6 <sup>1</sup> / <sub>2</sub>	0.520	1/2	0.820	1 <sup>3</sup> / <sub>16</sub>	3/4	10 <sup>1</sup> / <sub>8</sub>	3 <sup>1</sup> / <sub>2</sub>
×30 <sup>c</sup>	8.79	12.3	12 <sup>3</sup> / <sub>8</sub>	0.260	1/4	1/8	6.52	6 <sup>1</sup> / <sub>2</sub>	0.440	7/16	0.740	1 <sup>1</sup> / <sub>8</sub>	3/4	↓	↓
×26 <sup>c</sup>	7.65	12.2	12 <sup>1</sup> / <sub>4</sub>	0.230	1/4	1/8	6.49	6 <sup>1</sup> / <sub>2</sub>	0.380	3/8	0.680	1 <sup>1</sup> / <sub>16</sub>	3/4	↓	↓
W12×22 <sup>c</sup>	6.48	12.3	12 <sup>1</sup> / <sub>4</sub>	0.260	1/4	1/8	4.03	4	0.425	7/16	0.725	15/16	5/8	10 <sup>3</sup> / <sub>8</sub>	2 <sup>1</sup> / <sub>4</sub> <sup>d</sup>
×19 <sup>c</sup>	5.57	12.2	12 <sup>1</sup> / <sub>8</sub>	0.235	1/4	1/8	4.01	4	0.350	3/8	0.650	7/8	9/16	↓	↓
×16 <sup>c</sup>	4.71	12.0	12	0.220	1/4	1/8	3.99	4	0.265	1/4	0.565	13/16	9/16	↓	↓
×14 <sup>c,v</sup>	4.16	11.9	11 <sup>7</sup> / <sub>8</sub>	0.200	3/16	1/8	3.97	4	0.225	1/4	0.525	3/4	9/16	↓	↓

DIMENSIONS AND PROPERTIES

1-27

Table 1-1 (continued) W-Shapes Properties														 W12-W10	
Nom- inal Wt.	Compact Section Criteria		Axis X-X				Axis Y-Y				r <sub>ts</sub>	h <sub>o</sub>	Torsional Properties		
	b <sub>f</sub>	h	I	S	r	Z	I	S	r	Z			J	C <sub>w</sub>	
lb/ft	2t <sub>f</sub>	t <sub>w</sub>	in. <sup>4</sup>	in. <sup>3</sup>	in.	in. <sup>3</sup>	in. <sup>4</sup>	in. <sup>3</sup>	in.	in. <sup>3</sup>	in.	in.	in. <sup>4</sup>	in. <sup>6</sup>	
58	7.82	27.0	475	78.0	5.28	86.4	107	21.4	2.51	32.5	2.81	11.6	2.10	3570	
53	8.69	28.1	425	70.6	5.23	77.9	95.8	19.2	2.48	29.1	2.79	11.5	1.58	3160	
50	6.31	26.8	391	64.2	5.18	71.9	56.3	13.9	1.96	21.3	2.25	11.6	1.71	1880	
45	7.00	29.6	348	57.7	5.15	64.2	50.0	12.4	1.95	19.0	2.23	11.5	1.26	1650	
40	7.77	33.6	307	51.5	5.13	57.0	44.1	11.0	1.94	16.8	2.21	11.4	0.906	1440	
35	6.31	36.2	285	45.6	5.25	51.2	24.5	7.47	1.54	11.5	1.79	12.0	0.741	879	
30	7.41	41.8	238	38.6	5.21	43.1	20.3	6.24	1.52	9.56	1.77	11.9	0.457	720	
26	8.54	47.2	204	33.4	5.17	37.2	17.3	5.34	1.51	8.17	1.75	11.8	0.300	607	
22	4.74	41.8	156	25.4	4.91	29.3	4.66	2.31	0.848	3.66	1.04	11.9	0.293	164	
19	5.72	46.2	130	21.3	4.82	24.7	3.76	1.88	0.822	2.98	1.02	11.9	0.180	131	
16	7.53	49.4	103	17.1	4.67	20.1	2.82	1.41	0.773	2.26	0.983	11.7	0.103	96.9	
14	8.82	54.3	88.6	14.9	4.62	17.4	2.36	1.19	0.753	1.90	0.961	11.7	0.0704	80.4	

# Provide the solution for the assignment – HW4

$$F_y = 50 \text{ ksi}$$

plastic modulus of the section,

$$W 12 \times 19 \rightarrow \text{Table 1-1 : } Z_x = 24.7 \text{ in}^3$$

Q1

Assume the beam is fully braced,  $L_b < L_p$  (zone 1)

$$M_n = M_p$$

nominal bending moment

$$(M_n)_x = Z_x F_y = (24.7 \text{ in}^3) (50 \frac{\text{kip}}{\text{in}^2}) = 1235 \text{ k-in}$$

Q2

$$\phi \text{ in bending : } 0.9$$

$$\phi M_n = 0.9 \times 1235 = 1111.5 \text{ k-in}$$

Q3

The factored bending resistance

# Provide the solution for the assignment – HW4

$$M_u \leq \phi M_n$$

The factored design moment

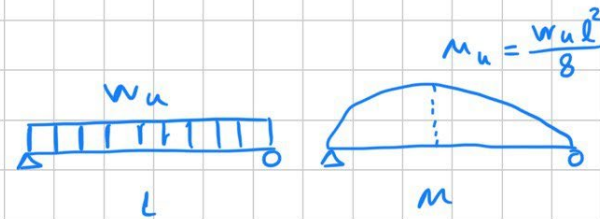
we Assume  $M_u$  equal to  $\phi M_n$

$$111.5 \text{ K-IN} \times \left(\frac{1}{12}\right) = 92.625 \text{ K-FT}$$

IN to FT

Q4

$$M_u = \frac{w_u l^2}{8}$$



$$92.625 = \frac{w_u \times 21^2}{8} \rightarrow w_u = \underline{\underline{1.68027 \text{ KLF}}}$$

Q5

The total factored design load,

# Provide the solution for the assignment – HW4

Total unfactored Dead load: Floor DL + beam selfweight

$$10 \text{ psf} \times \frac{2(\text{Span B})}{2} + 19 \text{ plf} = 159 \text{ PLF} \xrightarrow{\times \frac{1}{1000}} 0.159 \text{ KLF}$$

unit conversion

Q6

Factored DL :  $1.2 \times 0.159 = 0.1908$

Q7

$$W_u = 1.2 W_{DL} + 1.6 W_{LL}$$

$$1.68027 = 1.2 (0.159) + 1.6 (W_{LL})$$

$$\rightarrow 1.6 W_{LL} = 1.98947 \text{ KLF}$$

Factored Live load

Q8

$$W_{LL} = 0.9309 \text{ KLF}$$

Actual live load

Q9

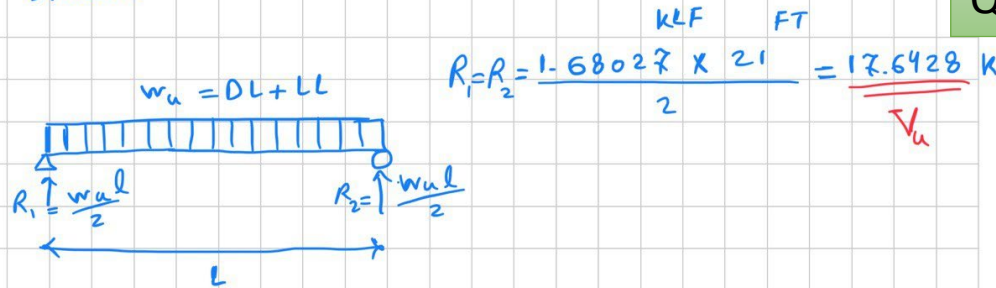
$$\frac{W_{LL}}{\text{Span B}} = \frac{0.9309 \text{ KLF}}{14} = 0.06649 \times 1000 = 66.49 \text{ PLF}$$

Q10



# Provide the solution for the assignment – HW4

Shear:



Q11

Zone 1:

**WEB YIELDING** (Most beam sections fall into this category)

$$\text{if } \frac{h}{t_w} \leq 2.45 \sqrt{E/F_y} = 59 \text{ (for 50 ksi steel)}$$

$$\text{then: } V_n = 0.6 F_y A_w$$

$$\left\{ \begin{array}{l} \text{if } \frac{h}{t_w} \leq 2.45 \sqrt{\frac{E}{F_y}} = 50 \text{ (for 50 KSI steel)} \\ V_n = 0.6 F_y A_w \end{array} \right.$$

$$\text{Table 1-1: } 46.2 < 50 \checkmark$$

$$A_w = d t_w = (12.2)(0.235) = 2.867 \text{ in}^2$$

Q12

$$V_n = 0.6 F_y A_w = 0.6(50)(2.867) = 86.01$$

Q13

$$\text{Check Shear: } V_u \leq V_n ?$$

$$17.6428 < 86.01 \checkmark \text{ o.k.}$$

Q14

# Provide the solution for the assignment – HW4

Deflection :

$$\text{limit } \frac{L}{180} = \frac{21 \times 12}{180} = (1.4) \text{ in}$$

Q16

$$\Delta_{\max} = \frac{5wL^4}{384EI} = \frac{5 \left( 1089.90 \times \frac{1}{12} \right) \times (21 \times 12)^4}{384 (29 \times 10^6) \left( \frac{16}{12} \right)} = 1.2650 \text{ in}$$

unfactored load DL+LL

Convert to IN

Table 1-7

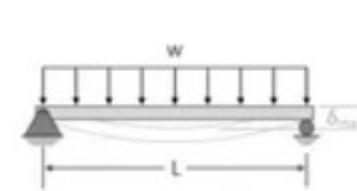
PSI

lb/in<sup>2</sup>

Q15

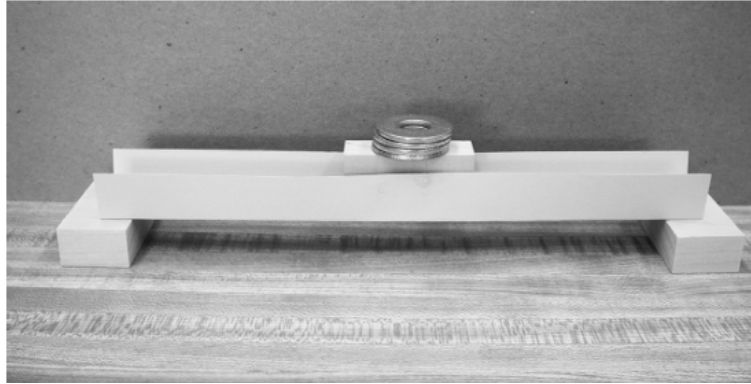
Total unfactored load → (DL) + (self-weight) + (LL)

$$140 + 19 + 930.9 = 1089.90 \text{ PLF}$$



$$\delta_{\max} = \frac{5wL^4}{384EI}$$

# Lab: Steel Beam Analysis



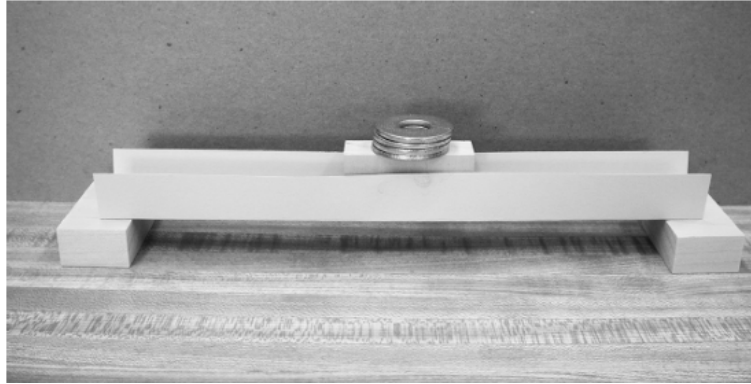
## Description

This project uses observation to understand how unbraced compression edges and lateral torsional buckling reduce the ultimate load capacity of steel beams.

## Goals

To observe the behavior of unbraced section edges in compression vs tension.  
To measure capacity loss due to lateral torsional buckling.

# Lab: Steel Beam Analysis



## Procedure

1. Position the U shaped section with the free edges on the upper side of the span.
2. Test how many washers the section can support at mid span. Use a wood block to position the load. Observe the mode (how) it fails.
3. Repeat the procedure with the section inverted and the free edges downward.
4. Compare the load level carried by each orientation of the paper beam and describe the behavior under load.

# Tower Project: How to start

## Criteria

- The tower is to be made of wood. Either **linear wood** (sticks) or **wood panels** (sheets) can be used. **Glue** can be used to connect the elements. **Gusset plates** at the joints are allowed and can also be glued. But no steel pins or fasteners may be used.
- Wood: **any species.** maximum **cross-sectional dimension** = **1/4"**.
- **NO** paper, mylar or plastic or string or dental floss.
- If a member is made by **laminating multiple pieces** together, the maximum cross-sectional dimension or thickness still cannot exceed 1/4".
- The **height of the tower = 48"**.
- The tower **must hold at least 50 lbs.**
- The entire tower **can weigh no more than 4 oz.**
- The top of the tower must be loadable. The weights will be stacked on top of the tower, but you may optionally use a loose piece of MDF or plywood as a tray under the weights. (It will not be counted in either weight or load)
- Towers will be graded on their low weight, high load-carrying capacity, and the load/weight ratio. The evaluation formula is:  
$$(4/\text{weight in OZ}) + (\text{load in LBS}/50) + (\text{load LBS}/\text{weight OZ}) \times 1.5$$
- The score will be normalized to a range of 50 to 100. It is used together with report scores to assess your project (a detailed evaluation form is given separately).



# Tower Project: How to start

Scoring	
Preliminary Report	40 pts
Testing	60 pts
Final Report	150 pts

## Procedure

1. Develop a structural concept for a tower meeting the above criteria.
2. Analyze the design concept with **either** hand calculations or a computer program (e.g. Dr. Frame)
3. Determine the capacity of the major members and of the overall tower (total capacity in LBS)
4. Estimate your expected score using the formula above.
5. Write the preliminary report.
6. Construct the structural model.
7. Test the model. 5-pound steel bars will be placed on top of the model, until the model fails. (bar size: 1 1/2" x 2" x 5 13/16").
8. Produce final report documenting requirements and process. See also score sheet.

Use NDS approach

Find load  $P$  and stress  $F'_c$  for each member

Use 1.0 for all factors except  $C_P$

Analysis

$$f_c = \frac{P}{A} \leq F'_c$$

Capacity

$$P = F'_c A$$

Design

$$A = \frac{P}{F'_c}$$



Arch324: STRUCTURES II

Thank you.

Any question?

Please feel free to ask questions.