

A green triangle is plotted on a coordinate plane. The vertices are located at $(-10, 0)$, $(-10, 10)$, and $(0, 0)$. The triangle is shaded green.

Recitation



5. Steel Beam Design

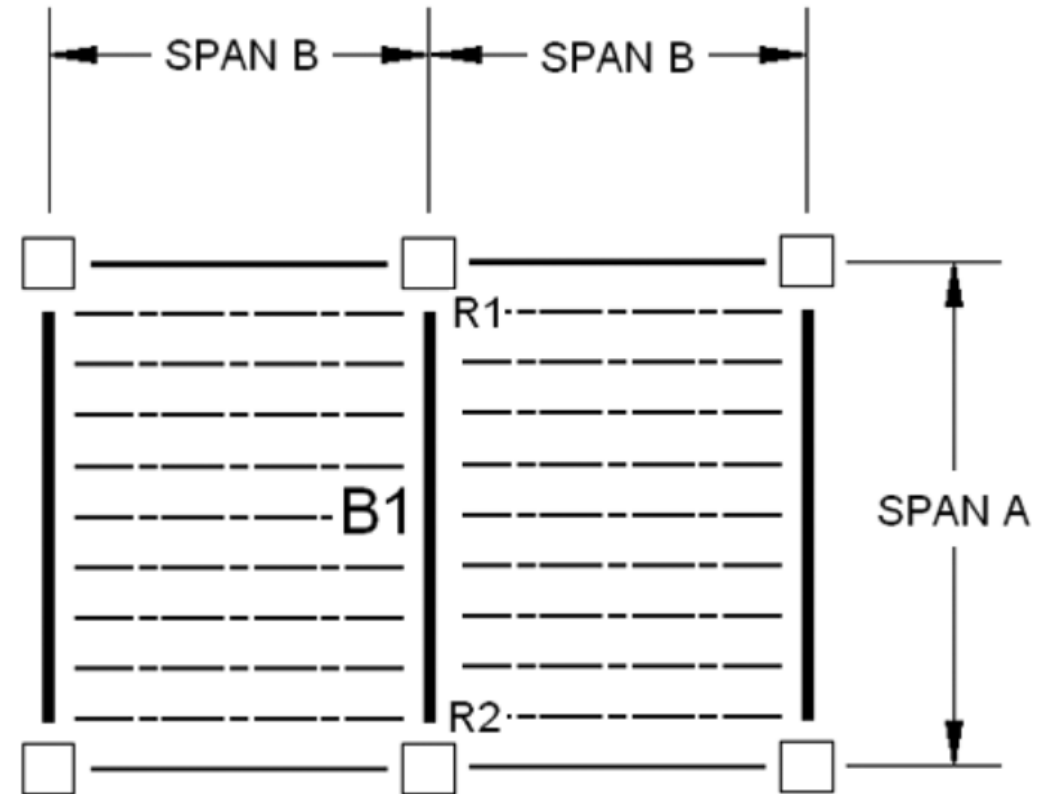
Choose the lightest steel W-section to support the applied dead and live floor loads on Beam B1. Choose a steel W-section from AISC Table 3-2 (posted on Canvas). For the selection of the beam, neglect selfweight (for loads marked with *). After selecting the lightest section from Table 3-2, revise the DL to include the beam selfweight. Check that the final M_u including selfweight is less than the beam strength, ϕM_n . Assume the beam is fully braced, $L_b < L_p$.

DATASET: 1

-2-

-3-

F_y	50 KSI
Span A	25 FT
Span B	17 FT
Floor Dead Load	14 PSF
Floor Live Load	90 PSF



Lightest section?

At first neglect beam self weight
The beam is fully braced → ZONE 1

#	Question	Your Response	Correct Answer	Score
1	The unfactored floor dead load on beam B1 (neglecting selfweight), w_{DL}^*	238 PLF	238 PLF	5
2	The unfactored floor live load on the beam, w_{LL}	1530 PLF	1530 PLF	5
3	The total factored design load on the beam (neglecting selfweight), w_u^*	2.73 KLF	2.7336 KLF	5
4	The factored design moment (neglecting selfweight), M_u^*	213.28 K-FT	213.5625 K-FT	5
5	The nominal bending moment (neglecting selfweight), M_n^*	2843.73 K-IN	2847.5 K-IN	5
6	The plastic modulus of the section (neglecting selfweight), Z_x^*	56.87 IN ³	56.95 IN ³	5
7	The nominal depth of the lightest passing W-section from Z_x table (include selfweight)	IN	SUBMIT	
8	The weight of the lightest passing W-section from Z_x table	58 PLF	35 PLF	0
9	The plastic modulus of the section for the chosen section, Z_x	IN ³	SUBMIT	
10	The revised unfactored dead load on the beam (including selfweight), w_{DL}	PLF	SUBMIT	
11	The total factored design load on the beam (including selfweight), w_u	KLF	SUBMIT	
12	The factored design moment (including selfweight), M_u in KIP-FT	K-FT	SUBMIT	
13	The factored design moment (including selfweight), M_u in KIP-IN	K-IN	SUBMIT	
14	The nominal factored bending moment for the chosen section, ϕM_n	K-IN	SUBMIT	

Unfactored Floor Dead load on beam B₁:

$$w_D = \underset{\text{PSF}}{14} \times 2 \left(\frac{\text{Span B}}{2} \right) = 238 \text{ PLf}$$

live load :

$$w_L = 90 \times 17 = 1530 \text{ PLf}$$

$w_u \rightarrow$ Total Factored Design load

$$w_u = 1.2 w_D + 1.6 w_L$$

$$w_u = 1.2(238) + 1.6(1530) = 285.6 + 2448 \Rightarrow$$

$$w_u = 2733.6 \times \frac{1}{1000} = 2.73 \text{ KLF}$$

A green triangle is plotted on a coordinate plane. The vertices are located at the coordinates $(-1, 0)$, $(-1, 2)$, and $(1, 1)$. The triangle is shaded green.

$$M_u \leq \emptyset M_n$$

Assume : $M_u = \emptyset M_n \rightarrow$ we want to use the maximum capacity

$$\phi = 0.9$$

$$M_u = \frac{M_u}{\phi} = \frac{213.28}{0.9} = 236.97 \text{ k-FT} \times 12 = 2843.73 \text{ k-IN}$$

Zone 1:

$$M_n = Z_x F_y \rightarrow 2843.73 = Z_x (50)$$

$$Z_x = 56.87$$

based on the Table 3-2:

W18x35

Z_x

Table 3-2 (continued)
W-Shapes
Selection by Z_x

$F_y = 50$ ksi

Shape	Z_x in. ³	M_{px}/Ω_b		M_{rx}/Ω_b		BF/Ω_b		L_p ft	L_r ft	I_x in. ⁴	V_{nx}/Ω_v	
		kip-ft	$\phi_b M_{px}$ LRFD	kip-ft	$\phi_b M_{rx}$ LRFD	kips	$\phi_b BF$ LRFD				kips	$\phi_v V_{nx}$ LRFD
		ASD	LRFD	ASD	LRFD	ASD	LRFD				ASD	LRFD
W18x35	66.5	166	249	101	151	8.14	12.3	4.31	12.3	510	106	159
W12x45	64.2	160	241	101	151	3.80	5.80	6.89	22.4	348	81.1	122
W16x36	64.0	160	240	98.7	148	6.24	9.36	5.37	15.2	448	93.8	141
W14x38	61.5	153	231	95.4	143	5.37	8.20	5.47	16.2	385	87.4	131
W10x49	60.4	151	227	95.4	143	2.46	3.71	8.97	31.6	272	68.0	102
W8x58	59.8	149	224	90.8	137	1.70	2.55	7.42	41.6	228	89.3	134
W12x40	57.0	142	214	89.9	135	3.66	5.54	6.85	21.1	307	70.2	105
W10x45	54.9	137	206	85.8	129	2.59	3.89	7.10	26.9	248	70.7	106
W14x34	54.6	136	205	84.9	128	5.01	7.55	5.40	15.6	340	79.8	120
W16x31	54.0	135	203	82.4	124	6.86	10.3	4.13	11.8	375	87.5	131
W12x35	51.2	128	192	79.6	120	4.34	6.45	5.44	16.6	285	75.0	113
W8x48	49.0	122	184	75.4	113	1.67	2.55	7.35	35.2	184	68.0	102
W14x30	47.3	118	177	73.4	110	4.63	6.95	5.26	14.9	291	74.5	112
W10x39	46.8	117	176	73.5	111	2.53	3.78	6.99	24.2	209	62.5	93.7
W16x26	44.2	110	166	67.1	101	5.93	8.98	3.96	11.2	301	70.5	106
W12x30	43.1	108	162	67.4	101	3.97	5.96	5.37	15.6	238	64.0	95.9

Revise dead load and include self weight

$$W_D = 238 \text{ PLF} + 35 \text{ PLF} = 273 \text{ PLF}$$

$$W_u = 1.2(273) + 1.6(1530) = 2775.6 \times \frac{1}{1000} = 2.77 \text{ klf}$$


$$M_u = \frac{w_u l^2}{8} = \frac{2.77(25)^2}{8} = 216.4 \text{ k-FT}$$

$$\text{unit Conversion : } 216.4 \times 12 = 2596.875$$

$$M_n = Z_x F_y = \underbrace{66.5}_{\substack{\downarrow \\ \text{based on Table}}} \times 50 = 3325$$

$$\phi M_n = 0.9(3325) = 2992.5$$

$$2992.5 > 2596.875$$

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- Thanks for your attention 😊