

Arch324

STRUCTURES II

Winter 2025
Recitation

FACULTY: Prof. Peter von Bülow
Mohsen Vatandoost

Arch324: STRUCTURES II

Welcome to Recitation session 02/21

Mohsen Vatandoost {Ph.D., M.Sc., M. Arch}

mohsenv@umich.edu

Office: Room 3122

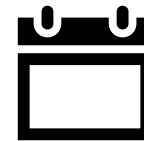
hours:

Fri: 11:30 – 12:30

Mon, Wed: 11:00 - 12:00

walk-ins welcome!

Please feel free to ask questions.



[Click here to make an appointment](#)

Where can you find me?



Arch324: STRUCTURES II

Welcome to Recitation session 02/21

Outline:

- Quick **Recap** of the week
- Provide the solution for the assignment (**Homework 5**)
- Answering student's questions
- Lab: **Steel Columns**
- **Tower Project:** Preliminary report (you will get feedback shortly/ Test date: March 24)

Please feel free to ask questions.

Recap of the week

Steel Beam **Design** Procedure (zone 1)

1. Use the maximum moment equation, and solve for the ultimate moment, M_u .
2. Set $\phi M_n = M_u$ and solve for M_n
3. Assume Zone 1 to determine Z_x required
4. Select the lightest beam with a Z_x greater than the Z_x required from AISC table
5. Determine if $h/t_w < 59$
(case 1, most common)
6. Determine A_w :
 $A_w = d t_w$
7. Calculate V_n :
 $V_n = 0.6 F_y A_w$
8. Calculate V_u for the given loading
 $V_u = w_u L / 2$ (e.g. unif. load)
9. Check $V_u < \phi V_n$
 ϕ for $V = 1.0$
10. Check deflection

Provide the solution for the assignment – HW4

- Problem:

5. Steel Beam Design

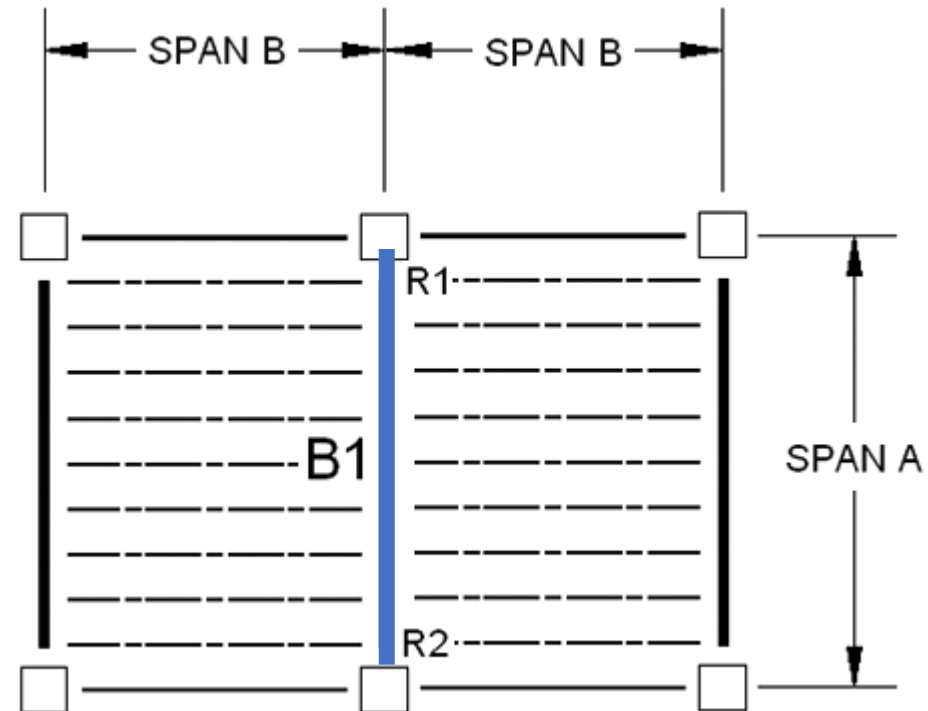
Choose the lightest steel W-section to support the applied dead and live floor loads on Beam B1. Choose a steel W-section from AISC Table 3-2 (posted on Canvas). For the selection of the beam, neglect selfweight (for loads marked with *). After selecting the lightest section from Table 3-2, revise the DL to include the beam selfweight. Check that the final M_u including selfweight is less than the beam strength, ϕM_n . Assume the beam is fully braced, $L_b < L_p$. (Zone 1)

DATASET: 1

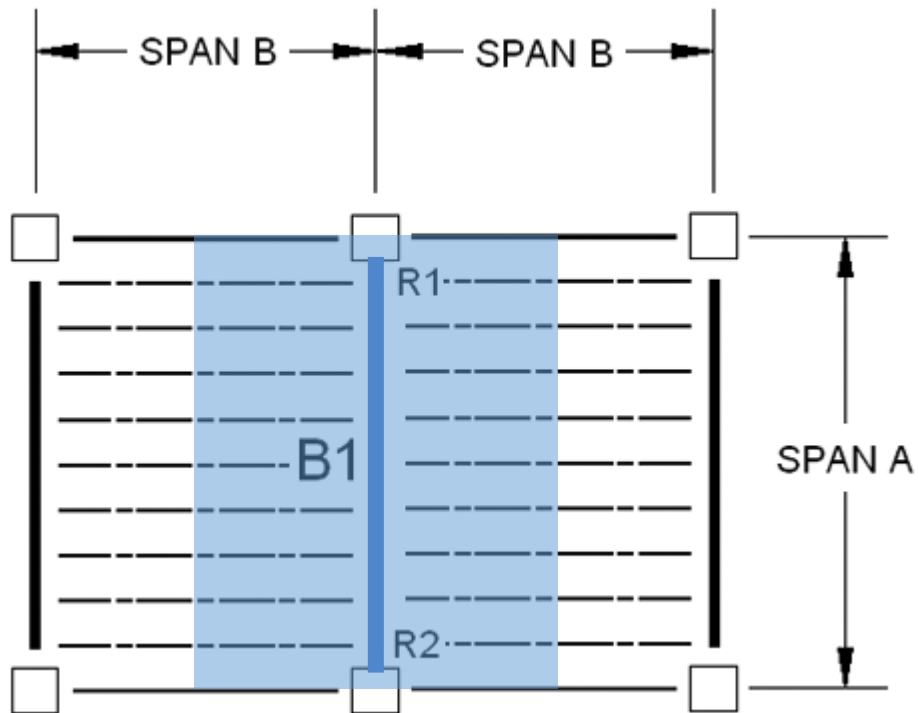
-2-

-3-

Fy	50 KSI
Span A	33 FT
Span B	15 FT
Floor Dead Load	18 PSF
Floor Live Load	80 PSF



Provide the solution for the assignment – HW4



#	Question	Your Response
1	The unfactored floor dead load on beam B1 (neglecting selfweight), w_{DL}^*	PLF
2	The unfactored floor live load on the beam, w_{LL}	PLF
3	The total factored design load on the beam (neglecting selfweight), w_u^*	KLF
4	The factored design moment (neglecting selfweight), M_u^*	K-FT
5	The nominal bending moment (neglecting selfweight), M_n^*	K-IN
6	The plastic modulus of the section (neglecting selfweight), Z_x^*	IN3
7	The nominal depth of the lightest passing W-section from Z_x table (include selfweight)	IN
8	The weight of the lightest passing W-section from Z_x table	PLF
9	The plastic modulus of the section for the chosen section, Z_x	IN3
10	The revised unfactored dead load on the beam (including selfweight), w_{DL}	PLF
11	The total factored design load on the beam (including selfweight), w_u	KLF
12	The factored design moment (including selfweight), M_u in KIP-FT	K-FT
13	The factored design moment (including selfweight), M_u in KIP-IN	K-IN
14	The nominal factored bending moment for the chosen section, ϕM_n	K-IN

Provide the solution for the assignment – HW5

un factored floor dead load on beam B1:

$$w_D = 18 \text{ PSF} \times 2 \left(\frac{\text{Span B}}{2} \right) = 270 \text{ PLF}$$

Q1

Live load :

$$w_L = 80 \times 15 = 1200 \text{ PLF}$$

Q2

w_u (Total factored design load):

$$w_u = 1.2 w_D + 1.6 w_L$$

$$w_u = 1.2 (270) + 1.6 (1200) = 2294 \text{ PLF} \times \frac{1}{1000} = 2.294 \text{ KLF}$$

Q3

Provide the solution for the assignment – HW5

Design moment

$$M_u = \frac{w_u L^2}{8}$$
$$= \frac{2.244 \times 33^2}{8} = \underline{305.4645 \text{ K-FT}}$$

Q4

nominal bending moment:

$$M_u \leq \phi M_n$$

Assumption: $M_u = \phi M_n \rightarrow$

Nominal bending moment

$$M_n = \frac{M_u}{\phi=0.9} = \frac{305.4645}{0.9} = \underline{339.405 \text{ K-FT}} \times 12 = 4072.86 \text{ K-IN}$$

Q5

unit conversion

Provide the solution for the assignment – HW5

The plastic modulus of the section

problem Assumption: fully braced (Zone 1)

$$M_n = Z_x F_y$$

4072.86 = $Z_x \cdot (50)$ Required $Z_x = 81.4572 \text{ in}^3$ Q6

K-IN in³ KSI(K-IN)

look up in the table:

from the bott go upward and find nearest Z
(choose Bold row) → lightest + strongest in the series

W21x44 → weight Q8

height depth → Z = 95.4 in³ Q9

Q7

Table 3-2 (continued)																		$F_y = 50 \text{ ksi}$		
W-Shapes																				
Selection by Z_x																				
Shape	Z_x	M_{px}/Ω_b		$\phi_b M_{px}$		M_{rx}/Ω_b		$\phi_b M_{rx}$		B_f/Ω_b		$\phi_b B_f$		L_p	L_r	I_x	V_{nx}/Ω_v		$\phi_v V_{nx}$	
		kip-ft	LRFD	kip-ft	LRFD	kip-ft	LRFD	kip-ft	LRFD	kip-ft	LRFD	kip	LRFD				kip	LRFD		
	in. ³	ASD	LRFD	ASD	LRFD	ASD	LRFD	ASD	LRFD	ASD	LRFD	ASD	LRFD	ft	ft	in. ⁴	ASD	LRFD	LRFD	
W21x44	95.4	238	358	143	214	11.1	16.8	4.45	13.0	843	145	217								
W16x50	92.0	230	345	141	213	7.69	11.4	5.62	17.2	659	124	186								
W18x46	90.7	226	340	138	207	9.63	14.6	4.56	13.7	712	130	195								
W14x53	87.1	217	327	136	204	5.22	7.93	6.78	22.3	541	103	154								
W12x58	86.4	216	324	136	205	3.82	5.69	8.87	29.8	475	87.8	132								
W10x68	85.3	213	320	132	199	2.58	3.85	9.15	40.6	394	97.8	147								
W16x45	82.3	205	309	127	191	7.12	10.8	5.55	16.5	586	111	167								
W18x40	78.4	196	294	119	180	8.94	13.2	4.49	13.1	612	113	169								
W14x48	78.4	196	294	123	184	5.09	7.67	6.75	21.1	484	93.8	141								
W12x53	77.9	194	292	123	185	3.65	5.50	8.76	28.2	425	83.5	125								
W10x60	74.6	186	280	116	175	2.54	3.82	9.08	36.6	341	85.7	129								
W16x40	73.0	182	274	113	170	6.67	10.0	5.55	15.9	518	97.6	146								
W12x50	71.9	179	270	112	169	3.97	5.98	6.92	23.8	391	90.3	135								
W8x67	70.1	175	263	105	159	1.75	2.59	7.49	47.6	272	103	154								
W14x43	69.6	174	261	109	164	4.88	7.28	6.68	20.0	428	83.6	125								
W10x54	66.6	166	250	105	158	2.48	3.75	9.04	33.6	303	74.7	112								
W18x35	66.5	166	249	101	151	8.14	12.3	4.31	12.3	510	106	159								
W12x45	64.2	160	241	101	151	3.80	5.80	6.89	22.4	348	81.1	122								
W16x36	64.0	160	240	98.7	148	6.24	9.36	5.37	15.2	448	93.8	141								
W14x38	61.5	153	231	95.4	143	5.37	8.20	5.47	16.2	385	87.4	131								
W10x49	60.4	151	227	95.4	143	2.46	3.71	8.97	31.6	272	68.0	102								
W8x58	59.8	149	224	90.8	137	1.70	2.55	7.42	41.6	228	89.3	134								
W12x40	57.0	142	214	89.9	135	3.66	5.54	6.85	21.1	307	70.2	105								
W10x45	54.9	137	206	85.8	129	2.59	3.89	7.10	26.9	248	70.7	106								
W14x34	54.6	136	205	84.9	128	5.01	7.55	5.40	15.6	340	79.8	120								
W16x31	54.0	135	203	82.4	124	6.86	10.3	4.13	11.8	375	87.5	131								
W12x35	51.2	128	192	79.6	120	4.34	6.45	5.44	16.6	285	75.0	113								
W8x48	49.0	122	184	75.4	113	1.67	2.55	7.35	35.2	184	68.0	102								
W14x30	47.3	118	177	73.4	110	4.63	6.95	5.26	14.9	291	74.5	112								
W10x39	46.8	117	176	73.5	111	2.53	3.78	6.99	24.2	209	62.5	93.7								
W16x26*	44.2	110	166	67.1	101	5.93	8.98	3.96	11.2	301	70.5	106								
W12x30	43.1	108	162	67.4	101	3.97	5.96	5.37	15.6	238	64.0	95.9								
ASD	LRFD	* Shape does not meet the h/t_w limit for shear in AISC Specification Section G2.1(a) with $F_y = 50 \text{ ksi}$; therefore, $\phi_v = 0.90$ and $\Omega_v = 1.67$.																		
$\Omega_b = 1.67$	$\phi_b = 0.90$																			
$\Omega_v = 1.50$	$\phi_v = 1.00$																			

Provide the solution for the assignment – HW5

revise the dead load and include self weight:

$$w_D = 270 \text{ PLF} + 44 \text{ PLF} = 314 \text{ PLF} \quad \text{Q10}$$

$$w_u = 1.2(314) + 1.6(1200) = 2296.8 \text{ PLF} \times \frac{1}{1000} = 2.2968 \text{ KLF} \quad \text{Q11}$$

Design moment

$$M_u = \frac{w_u L^2}{8} = \frac{2.2968 \times 33^2}{8} = 312.6519 \text{ K-FT} \quad \text{Q12}$$

$$\times 12 = 3751.8228 \text{ K-IN} \quad \text{Q13}$$

unit conversion

$$\phi M_n = \phi Z F_y = 0.9(95.4)(50) = 4293 \text{ K-IN} \quad \text{Q14}$$

$$4293 > 3751.82 \quad \text{O.K. } \checkmark$$

Lab: Steel Columns

Description

This project gives the opportunity to identify steel sections and determine their properties and strength using the AISC tables.

Goals

- To identify a steel section based on dimensions.
- To determine the sectional properties using AISC table
- To determine the load capacity based on AISC column table.

Procedure

1. Measure the steel column section shown below. (your GSI will tell you which one)
2. Based on the sectional dimensions find the shape in the steel table.
3. Use the column table and the given height to find the load capacity. Both columns are A-36 steel ($F_y = 36$ ksi).



L = 15 ft. – 4 in.

or



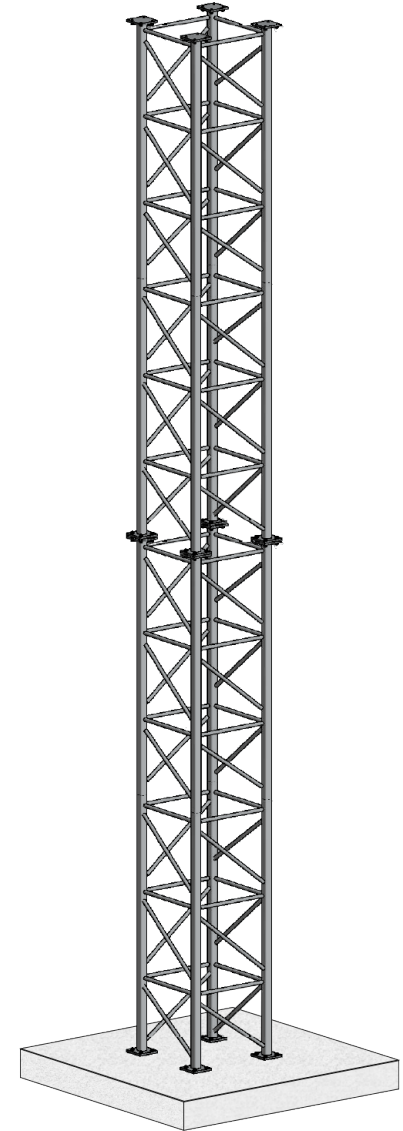
L = 13 ft. 4 in.

Tower Project: Prelim Report Guidelines 2024

Tower Project – Preliminary Report Requirements

Explanation – describe how the design was developed, the basis of the structural concept, and how the principles of column behavior influenced the design decisions.

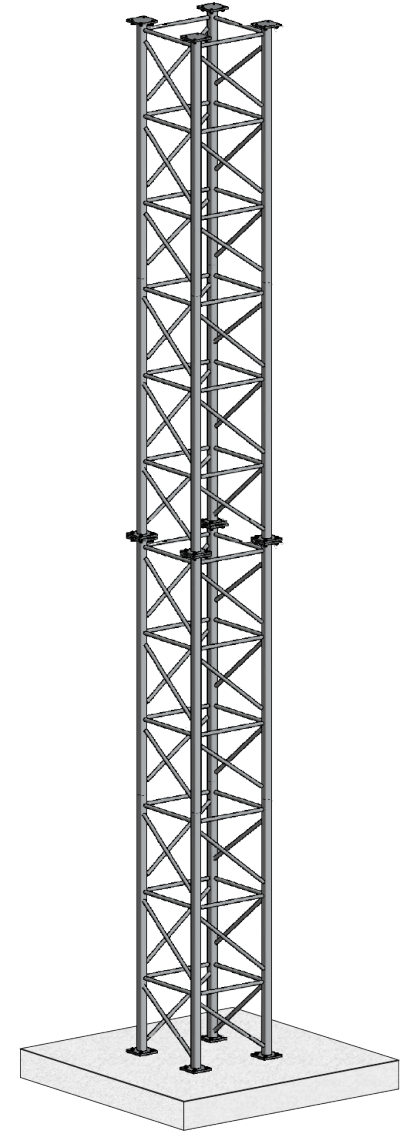
Illustration – include diagrams/drawings that describe the structure in its entirety. **At least a horizontal cross-section and an elevation of the tower are required.** Dimensions are to be included and the member sizes labeled.



Tower Project: Prelim Report Guidelines 2024

The report should include the following:

- Choose **wood type** and stress properties
- Determine the **cross-sectional area** of each member
(Find the axial force P and the allowable stress F'_c .)
Then size the members based on the force in each member.
- Predict the **total weight** of the tower.
The total weight should be under **4 OZ.**
- Predict **Capacity**
 - **Construct a table**, for each member type
(e.g. main vertical, horizontal tie, diagonal brace)
 - **calculate the ratio of f_c/F'_c**
(This ratio should be below 1.0 for all members.)
- Calculate the **buckling capacity** of the tower as a whole.
This is done by treating the tower as one column loaded at the top



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Thank you.

Any question?

Please feel free to ask questions.