

# Arch 324

# Structures II

Winter 2026 Recitation 004

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# Recitation 004

Welcome to session 4!

- Quick Lecture Recap
- Homework #4 Steel Beam Analysis
- Tower
- Lab: None

*Feel free to ask questions anytime*

# Lecture: Properties of Steel

Architecture 324

Structures II

## Steel Beam Analysis

- Steel Codes: ASD vs. LRFD
- Analysis Methods



# Lecture: Steel Beam Analysis

## Procedure - Analysis of Steel Beams – for Zone 1 $L_b < L_p$ Pass/Fail

Given: yield stress, steel section, loading, bracing ( $L_b$ )

Find: pass/fail of section

1. Calculate the factored design load  $w_u$   
 $w_u = 1.2W_{DL} + 1.6W_{LL}$

2. Determine the design moment  $M_u$ .  
 $M_u$  will be the maximum beam moment using the factored loads

3. Insure that  $L_b < L_p$  (zone 1)  
 $L_p = 1.76 r_y \sqrt{E/F_y}$

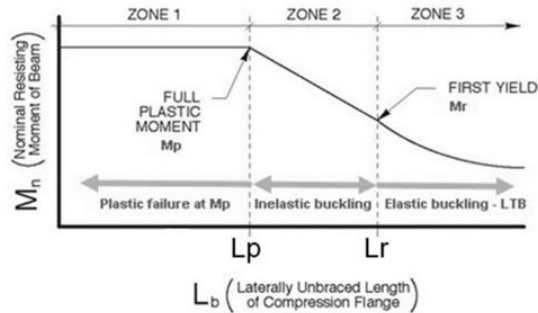
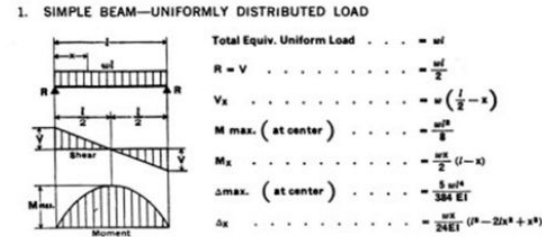
4. Determine the nominal moment,  $M_n$   
 $M_n = F_y Z_x$  (look up  $Z_x$  for section)

5. Factor the nominal moment  
 $\phi M_n = 0.90 M_n$

6. Check that  $M_u < \phi M_n$

7. Check shear

8. Check deflection



# Lecture: Steel Beam Analysis

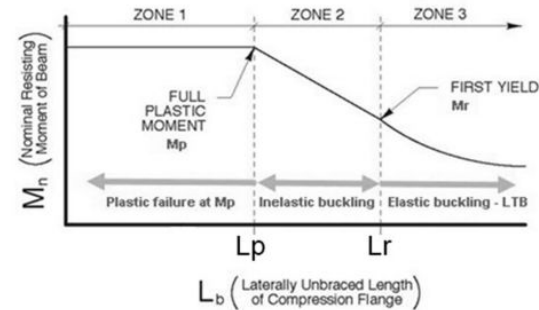
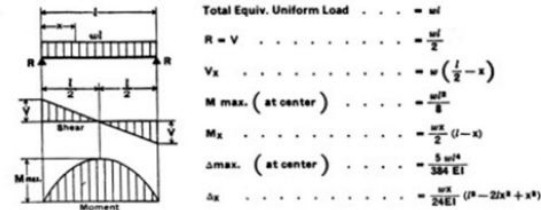
## Procedure - Analysis of Steel Beam - Capacity

Given: yield stress, steel section, bracing

Find: moment or load capacity

1. Determine the unbraced length of the compression flange ( $L_b$ ).
2. Find the  $L_p$  and  $L_r$  values from the AISC  $Z_x$  Table 3-2
3. Compare  $L_b$  to  $L_p$  and  $L_r$  and determine which equation for  $M_n$  or  $M_{cr}$  to be used.
4. Determine the beam load equation for maximum moment in the beam.
5. Calculate load based on maximum moment.  $M_u = \phi_b M_n$

1. SIMPLE BEAM—UNIFORMLY DISTRIBUTED LOAD



# HW #4: Steel Beam Design

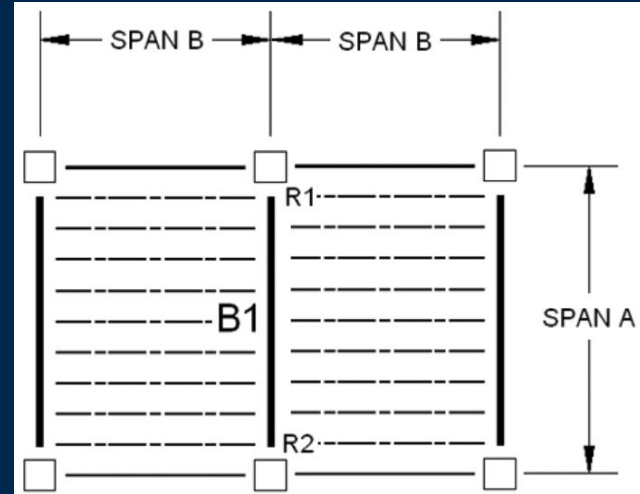
Analyze the given W-section for beam B1 to determine the maximum live load capacity the floor can carry. Determine the shear and bending forces and check the maximum deflection against an allowable of  $L/180$ . Assume the beam is fully braced,  $L_b < L_p$  (zone 1).

DATASET: 1

-2-

-3-

W-section	W10X30
Fy	50 KSI
Span A	18 FT
Span B	12 FT
Floor DL	14 PSF



# HW #4: Steel Beam Design

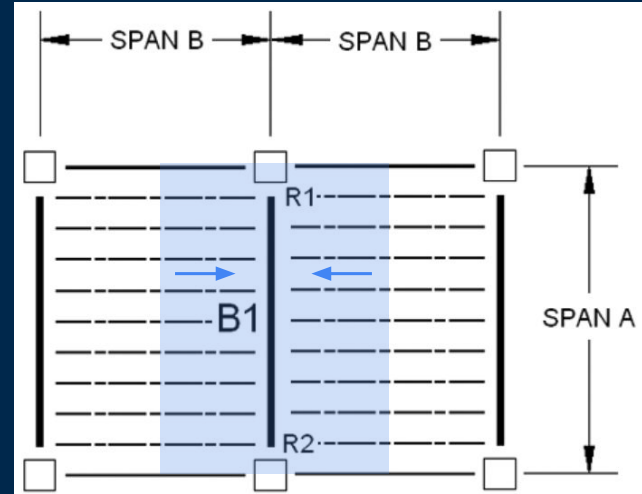
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-2-

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# HW #4: Steel Beam Design

1-26

DIMENSIONS AND PROPERTIES

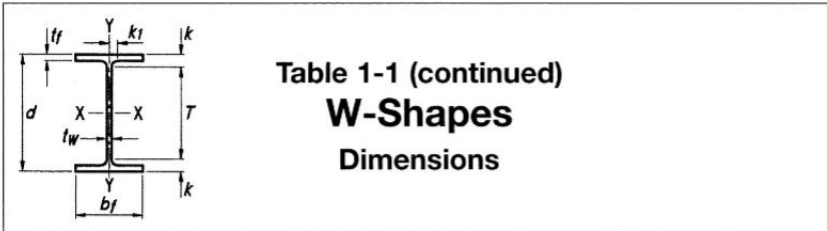


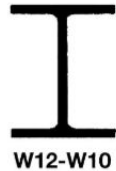
Table 1-1 (continued)  
W-Shapes  
Dimensions

Shape	Area, A in. <sup>2</sup>	Depth, d in.	Web			Flange			Distance						
			Thickness, $t_w$ in.	$\frac{t_w}{2}$ in.	Width, $b_f$ in.	Thickness, $t_f$ in.	$k$		$k_1$ in.	$T$ in.	Workable Gage in.				
							$k_{des}$ in.	$k_{det}$ in.							
W10×30	8.84	10.5	10 <sup>1</sup> / <sub>2</sub>	0.300	<sup>3</sup> / <sub>16</sub>	<sup>3</sup> / <sub>16</sub>	5.81	5 <sup>3</sup> / <sub>4</sub>	0.510	<sup>1</sup> / <sub>2</sub>	0.810	1 <sup>1</sup> / <sub>8</sub>	1 <sup>1</sup> / <sub>16</sub>	8 <sup>1</sup> / <sub>4</sub>	2 <sup>3</sup> / <sub>4</sub> <sup>9</sup>
×26	7.61	10.3	10 <sup>3</sup> / <sub>8</sub>	0.260	<sup>1</sup> / <sub>4</sub>	<sup>1</sup> / <sub>8</sub>	5.77	5 <sup>3</sup> / <sub>4</sub>	0.440	<sup>7</sup> / <sub>16</sub>	0.740	1 <sup>1</sup> / <sub>16</sub>	1 <sup>1</sup> / <sub>16</sub>	↓	↓
×22 <sup>c</sup>	6.49	10.2	10 <sup>1</sup> / <sub>8</sub>	0.240	<sup>1</sup> / <sub>4</sub>	<sup>1</sup> / <sub>8</sub>	5.75	5 <sup>3</sup> / <sub>4</sub>	0.360	<sup>3</sup> / <sub>8</sub>	0.660	1 <sup>5</sup> / <sub>16</sub>	5 <sup>1</sup> / <sub>8</sub>	↓	↓

DIMENSIONS AND PROPERTIES

1-27

Table 1-1 (continued)  
W-Shapes  
Properties



Nominal Wt. lb/ft	Compact Section Criteria		Axis X-X					Axis Y-Y				$r_{ts}$ in.	$h_o$ in.	Torsional Properties	
	$\frac{b_f}{2t_f}$	$\frac{h}{t_w}$	$I$ in. <sup>4</sup>	$S$ in. <sup>3</sup>	$r$ in.	$Z$ in. <sup>3</sup>	$I$ in. <sup>4</sup>	$S$ in. <sup>3</sup>	$r$ in.	$Z$ in. <sup>3</sup>	$J$ in. <sup>4</sup>			$C_w$ in. <sup>6</sup>	
	30	5.70	29.5	170	32.4	4.38	36.6	16.7	5.75	1.37	8.84	1.60	10.0	0.622	414
26	6.56	34.0	144	27.9	4.35	31.3	14.1	4.89	1.36	7.50	1.58	9.86	0.402	345	
22	7.99	36.9	118	23.2	4.27	26.0	11.4	3.97	1.33	6.10	1.55	9.84	0.239	275	

# HW #4: Steel Beam Design

1-26

DIMENSIONS AND PROPERTIES

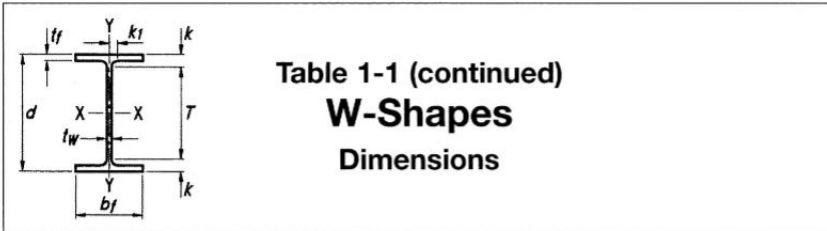


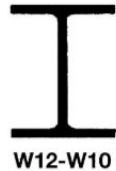
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			Thickness, <i>t<sub>w</sub></i> in.	$\frac{t_w}{2}$ in.	Width, <i>b<sub>f</sub></i> in.	Thickness, <i>t<sub>f</sub></i> in.	<i>k</i>		<i>T</i> in.						
							<i>k<sub>des</sub></i> in.	<i>k<sub>det</sub></i> in.							
W10×30	8.84	10.5	10 <sup>1</sup> / <sub>2</sub>	0.300	<sup>5</sup> / <sub>16</sub>	<sup>3</sup> / <sub>16</sub>	5.81	5 <sup>3</sup> / <sub>4</sub>	0.510	<sup>1</sup> / <sub>2</sub>	0.810	1 <sup>1</sup> / <sub>8</sub>	1 <sup>1</sup> / <sub>16</sub>	8 <sup>1</sup> / <sub>4</sub>	2 <sup>3</sup> / <sub>4</sub> <sup>9</sup>
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DIMENSIONS AND PROPERTIES

1-27

Table 1-1 (continued)  
**W-Shapes**  
Properties



Nominal Wt. lb/ft	Compact Section Criteria $\frac{b_f}{2t_f}$ $\frac{h}{t_w}$		Axis X-X				Axis Y-Y				<i>r<sub>ts</sub></i> in.	<i>h<sub>o</sub></i> in.	Torsional Properties	
			<i>I</i> in. <sup>4</sup>	<i>S</i> in. <sup>3</sup>	<i>r</i> in.	<i>Z</i> in. <sup>3</sup>	<i>I</i> in. <sup>4</sup>	<i>S</i> in. <sup>3</sup>	<i>r</i> in.	<i>Z</i> in. <sup>3</sup>			<i>J</i> in. <sup>4</sup>	<i>C<sub>w</sub></i> in. <sup>6</sup>
26	6.56	34.0	144	27.9	4.35	31.3	14.1	4.89	1.36	7.50	1.58	9.86	0.402	345
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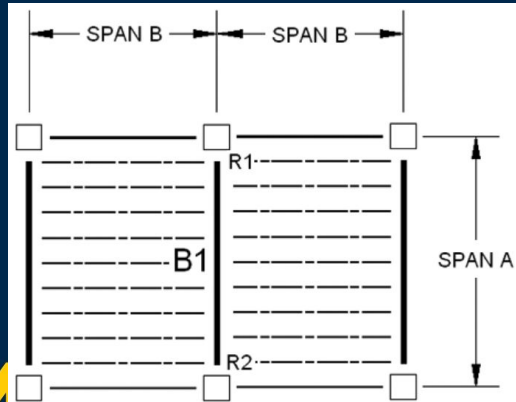
Q1

# HW #4: Steel Beam Design

Analyze the given W-section for beam B1 to determine the maximum live load capacity the floor can carry. Determine the shear and bending forces and check the maximum deflection against an allowable of  $L/180$ . Assume the beam is fully braced,  $L_b < L_p$  (zone 1).

DATASET: 1   -2-   -3-

W-section	W10X30
$F_y$	50 KSI
Span A	18 FT
Span B	12 FT
Floor DL	14 PSF



2. Nominal bending moment

$$M_n = Z_x (F_y)$$

$$= 36.6 (50)$$

$$= \boxed{1,830 \text{ k-in}} \leftarrow \#2$$

$$\text{in}^3 \times \frac{\text{k}}{\text{in}^2} = \frac{\text{k}}{\text{in}}$$

3. Factored bending resistance

$$\phi = 0.9$$

$$\phi M_n = 0.9 (M_n)$$

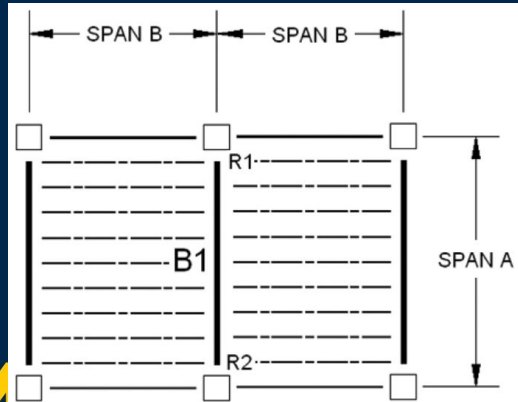
$$= 0.9 (1830 \text{ k-in})$$

$$= \boxed{1,647 \text{ k-in}} \leftarrow \#3$$

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DATASET: 1	-2-	-3-
W-section	W10X30	
Fy	50 KSI	
Span A	18 FT	
Span B	12 FT	
Floor DL	14 PSF	



4.  $M_u \leq \phi M_n$   
\* assume  $M_u = \phi M_n$ \*  
 $1.647 \left( \frac{1}{12} \right) = 139.25 \text{ k-ft} \leftarrow \#4$   
convert!  
in  $\rightarrow$  ft

5.  $M_u = \frac{w_u l^2}{8}$   
 $139.25 = \frac{w_u (18')^2}{8}$   
 $8(139.25) \downarrow 324 w_u$   
 $\frac{1,098}{324} = \frac{324 w_u}{324}$   
 $w_u = 3.39 \text{ kLF} \leftarrow \#5$

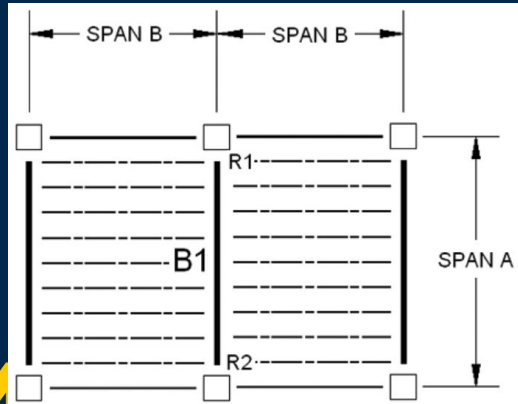
The diagram shows a simply supported beam of length  $l$  with a uniformly distributed load  $w_u$ . The beam is supported by a pin at the left end and a roller at the right end. The load is represented by a series of downward arrows. The beam is labeled M.

# HW #4: Steel Beam Design

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DATASET: 1   -2-   -3-

W-section	W10X30
Fy	50 KSI
Span A	18 FT
Span B	12 FT
Floor DL	14 PSF



6. Total unfactored dead load = floor DL + beam selfweight

$$DL \times 2 \left( \frac{\text{span } B}{2} \right) + 30 =$$

*PSF*                      *PLF*                      *PLF*

$$14(12) + 30 = \underline{198 \text{ PLF}}$$
  
$$198 \text{ PLF} \times \frac{1}{1000} = \boxed{0.198 \text{ KLF}} \leftarrow \#6$$

*convert!*

7. Factored dead load

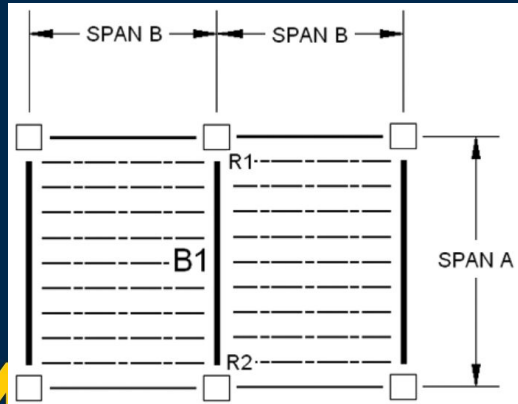
$$1.2(0.198) = \boxed{0.2376 \text{ KLF}} \leftarrow \#7$$

# HW #4: Steel Beam Design

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DATASET: 1   -2-   -3-

W-section	W10X30
$F_y$	50 KSI
Span A	18 FT
Span B	12 FT
Floor DL	14 PSF



8-9  $w_u = 1.2w_{DL} + 1.6w_{LL}$   
 $3.39 = 1.2(0.198) + 1.6w_{LL}$   
 $3.1524 = 1.6w_{LL}$   
 $w_{LL} = 1.97 \text{ KLF}$   
\* Actual live load \* #9

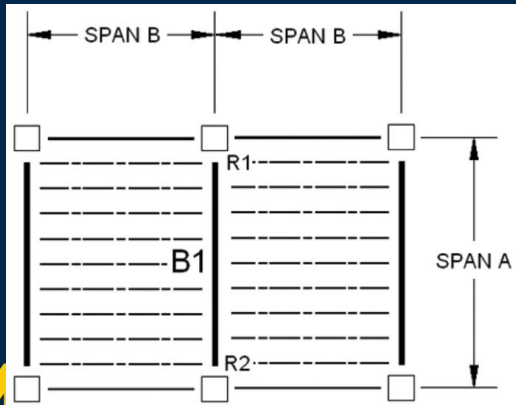
$1.6w_{LL} = 3.1524 \text{ KLF}$   
\* Factored live load \* #8

10.  $\frac{w_{LL}}{\text{Span B}} = \frac{1.97}{12} = 0.16417 \times 1000 = 164.17 \text{ PSF}$   
↑ convert! #10

# HW #4: Steel Beam Design

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DATASET: 1	-2-	-3-
W-section	W10X30	
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11. Max factored shear force

$w_u = DL + LL$

$R_1 = R_2 = \frac{w_u L}{2}$  (span A)

$= \frac{3.39 (18)}{2} = 30.51 \text{ K} = V_u$  #11

12.  $A_w = d(t_w) = 10.5" (0.3") = 3.15 \text{ in}^2$  ← #12

13.  $V_n = 0.6(F_y)(A_w) = 0.6(50)(3.15) = 94.5 \text{ K}$  ← #13

Check shear:  $V_u \leq V_n$  ?

$30.51 \text{ K} \leq 94.5 \text{ K}$

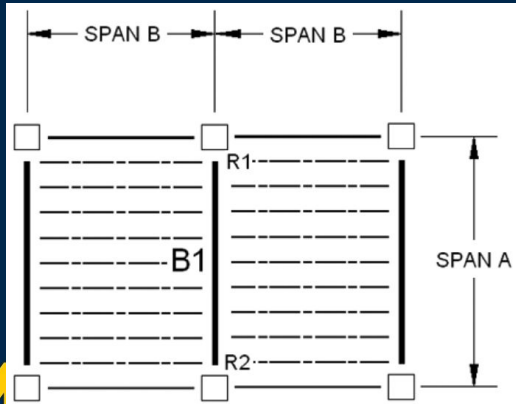
✓

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15 Actual Deflection

total unfactored load = DL + beam self weight + LL  
 $168 + 30 + 1,970$   
 $= 2,168 \text{ PLF}$

$\Delta_{max} = \frac{5w l^4}{384EI} = \frac{5(2,168 \times \frac{1}{2})(18 \times 12)^4}{384(29 \times 10^6)(170)} = 1.0385 \text{ in} \leftarrow \#15$

16. Deflection limit

$\frac{L}{180} = \frac{18' \times 12}{180} = \frac{216}{180} = 1.2 \text{ in}$

1.2 > 1.0385 ✓  
 limit      actual

Q17

Section safe for deflection = 1

# HW #4: Steel Beam Design

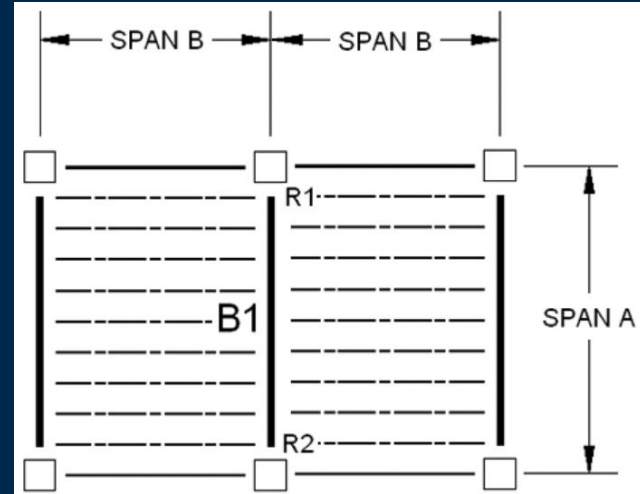
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DATASET: 1

-2-

-3-

W-section	W10X30
Fy	50 KSI
Span A	18 FT
Span B	12 FT
Floor DL	14 PSF



# Tower

## Due Dates:

- **Preliminary Report - 2.13 (next Friday!!)**
- Bridge Testing - 03.23 (Monday)
- Final Report - 04.17 (Sunday)

## Scoring:

- See rubric linked on website for more specifics
- 40 points = prelim report
- 60 points = performance
  - Meet requirements = 30pts
  - Efficiency = 30pts
- 150 points = final report
- 250 pts total!

# Tower

## Key Rules:

- Wood + glue only!
- Max cross-section =  $\frac{1}{4}$ " even when laminating multiple pieces together
- Height of tower = 48"
- Weight no more than 4oz
- Must hold at least 50lbs
- Load on top of the tower\*

\*You are allowed to use a loose piece of MDF or plywood as a tray to stack weights (wont count toward total weight/load)

# Tower

## How to Start:

- Get with your group!!
- Review examples
- Consider wood
  - Type will affect strength→weight ratio
- Get working on prelim asap!! :O

**No lab today** - have a great weekend :)