

Arch324

STRUCTURES II

Winter 2026
Recitation

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Recitation Guidelines

Homework Problem

Lab (No calculation, just an experiment)

- Please complete the lab sheet during recitation and hand it in before leaving.
- Try to attend all sessions. Unexcused absences will **affect your grade** starting from the second missed class.

Analysis Example - HW5

5. Steel Beam Design

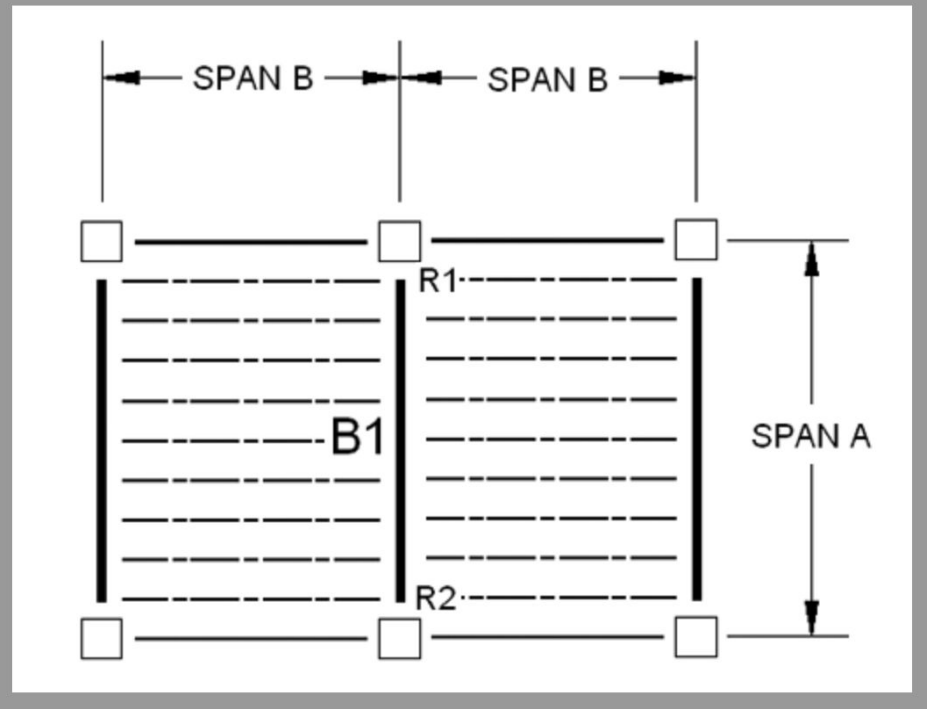
Choose the lightest steel W-section to support the applied dead and live floor loads on Beam B1. Choose a steel W-section from AISC Table 3-2 (posted on Canvas). For the selection of the beam, neglect selfweight (for loads marked with *). After selecting the lightest section from Table 3-2, revise the DL to include the beam selfweight. Check that the final Mu including selfweight is less than the beam strength, ϕM_n . Assume the beam is fully braced, $L_b < L_p$.

DATASET: 1

-2-

-3-

Fy	50 KSI
Span A	27 FT
Span B	14 FT
Floor Dead Load	19 PSF
Floor Live Load	90 PSF



Analysis Example - HW5

14 Questions

#	Question	Your Response
1	The unfactored floor dead load on beam B1 (neglecting selfweight), w_{DL}^*	<input type="text"/> PLF
2	The unfactored floor live load on the beam, w_{LL}	<input type="text"/> PLF
3	The total factored design load on the beam (neglecting selfweight), w_u^*	<input type="text"/> KLF
4	The factored design moment (neglecting selfweight), M_u^*	<input type="text"/> K-FT
5	The nominal bending moment (neglecting selfweight), M_n^*	<input type="text"/> K-IN
6	The plastic modulus of the section (neglecting selfweight), Z_x^*	<input type="text"/> IN3
7	The nominal depth of the lightest passing W-section from Z_x table (include selfweight)	<input type="text"/> IN
8	The weight of the lightest passing W-section from Z_x table	<input type="text"/> PLF
9	The plastic modulus of the section for the chosen section, Z_x	<input type="text"/> IN3
10	The revised unfactored dead load on the beam (including selfweight), w_{DL}	<input type="text"/> PLF
11	The total factored design load on the beam (including selfweight), w_u	<input type="text"/> KLF
12	The factored design moment (including selfweight), M_u in KIP-FT	<input type="text"/> K-FT
13	The factored design moment (including selfweight), M_u in KIP-IN	<input type="text"/> K-IN
14	The nominal factored bending moment for the chosen section, ϕM_n	<input type="text"/> K-IN

Answer HW5

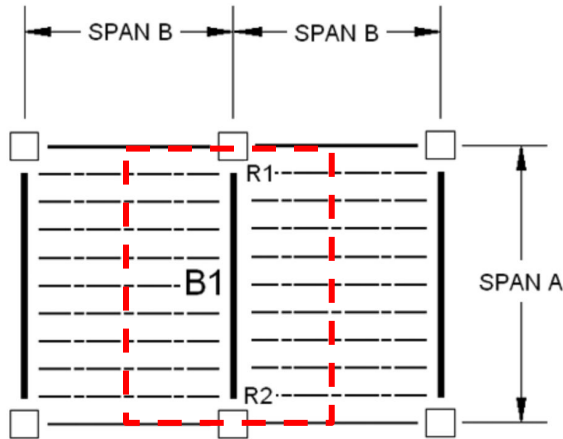
14 Questions

#	Question	Correct Answer
1	The unfactored floor dead load on beam B1 (neglecting selfweight), w_{DL}^*	266 PLF
2	The unfactored floor live load on the beam, w_{LL}	1260 PLF
3	The total factored design load on the beam (neglecting selfweight), w_u^*	2.3352 KLF
4	The factored design moment (neglecting selfweight), M_u^*	212.7951 K-FT
5	The nominal bending moment (neglecting selfweight), M_n^*	2837.268 K-IN
6	The plastic modulus of the section (neglecting selfweight), Z_x^*	56.74536 IN ³
7	The nominal depth of the lightest passing W-section from Z_x table (include selfweight)	18 IN
8	The weight of the lightest passing W-section from Z_x table	35 PLF
9	The plastic modulus of the section for the chosen section, Z_x	66.5 IN ³
10	The revised unfactored dead load on the beam (including selfweight), w_{DL}	301 PLF
11	The total factored design load on the beam (including selfweight), w_u	2.3772 KLF
12	The factored design moment (including selfweight), M_u in KIP-FT	216.62235 K-FT
13	The factored design moment (including selfweight), M_u in KIP-IN	2599.4682 K-IN
14	The nominal factored bending moment for the chosen section, ϕM_n	2992.5 K-IN

Analysis Example - HW5

Q1-Q3

Span A	27 FT
Span B	14 FT
Floor Dead Load	19 PSF
Floor Live Load	90 PSF

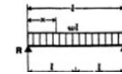


Procedure - Analysis of Steel Beams – for Zone 1 $L_b < L_p$ Pass/Fail

Given: yield stress, steel section, loading, bracing (L_b)
Find: pass/fail of section

- Calculate the factored design load w_u
 $w_u = 1.2W_{DL} + 1.6W_{LL}$

1. SIMPLE BEAM—UNIFORMLY DISTRIBUTED LOAD



Total Equiv. Uniform Load w
 $R = V$ $\frac{wL}{2}$
 V_x $w(\frac{L}{2} - x)$

$$\text{Tributary area} = \left(\frac{\text{Span B}}{2} + \frac{\text{Span B}}{2} \right) \cdot \text{Span A} = \left(\frac{14}{2} + \frac{14}{2} \right) \times 27 = 378 \text{ FT}^2$$

Q1 $W_{DL}^* = \text{Floor DL} \left(\frac{\text{Tributary area}}{\text{Span A}} \right) = 19 \left(\frac{378}{27} \right) = 266 \text{ PLF}$

Q2 $W_{LL} = \text{Floor LL} \left(\frac{\text{Tributary area}}{\text{Span A}} \right) = 90 \left(\frac{378}{27} \right) = 1260 \text{ PLF}$

$$W_u^* = 1.2 W_{DL}^* + 1.6 W_{LL} = 1.2 \times 266 + 1.6 \times 1260 = 2335.2 \text{ PLF}$$

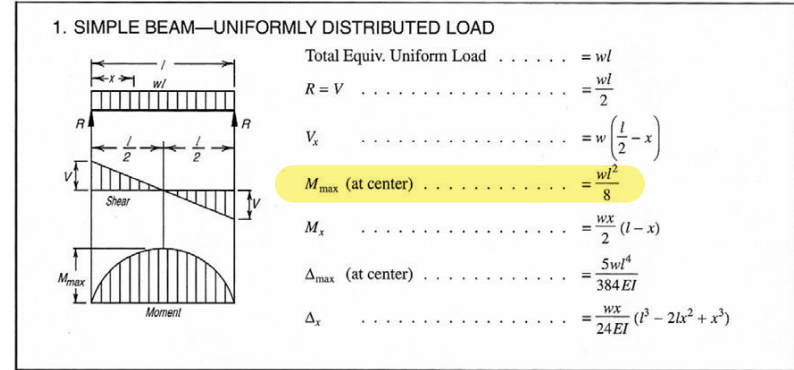
Q3 $= 2,335.2 \text{ KLF}$

Analysis Example - HW5

Q4-Q5

Design of Steel Beam – Procedure (zone 1)

1. Use the maximum moment equation, and solve for the ultimate moment, M_u .
2. Set $\phi M_n = M_u$ and solve for M_n



Span A=27 FT

Q4
$$M_u^* = \frac{W_u^* \cdot l^2}{8} = \frac{2.3352 (27)^2}{8} = 212.7951 \text{ K-FT}$$

Q5
$$\phi M_n = 0.9 \cdot M_n^* = 212.7951 \rightarrow M_n^* = \frac{212.7951}{0.9} \times 12 = 2837.268 \text{ K-IN}$$

Transfer to inch

Analysis Example - HW5

F_y

50 KSI

Q6-Q9 AISC14_Table3-2

3. Assume Zone 1 to determine Z_x required
4. Select the lightest beam with a Z_x greater than the Z_x required from AISC table

Q6

$$Z_x^* = \frac{M_n^*}{F_y} = \frac{2837.268}{50} = 56.74536 \text{ in}^3$$

→ select W18 X 35

Q7 Q8

Find the region in the **ZX** column where **ZX > 56.7** (blue region), then within this region identify the lightest beam (red region). **35** is the smallest of the right-hand values in the **Shape** column, so it is the lightest.

Q9 Z_x=66.5 in³

Z_x

Table 3-2 (continued)
W-Shapes
Selection by Z_x

F_y = 50 ksi

Shape	Z _x in. ³	M _{px} /Ω _b		M _{rx} /Ω _b		BF/Ω _b		L _p ft	L _r ft	I _x in. ⁴	V _{nx} /Ω _v	
		ASD kip-ft	LRFD kip-ft	ASD kip-ft	LRFD kip-ft	ASD kips	LRFD kips				ASD kips	LRFD kips
W18×35	66.5	166	249	101	151	8.14	12.3	4.31	12.3	510	106	159
W12×45	64.2	160	241	101	151	3.80	5.80	6.89	22.4	346	81.1	122
W16×36	64.0	160	240	98.7	148	6.24	9.36	5.37	15.2	448	93.8	141
W14×38	61.5	153	231	95.4	143	5.37	8.20	5.47	16.2	385	87.4	131
W10×49	60.4	151	227	95.4	143	2.46	3.71	8.97	31.6	272	68.0	102
W8×58	59.8	149	224	90.8	137	1.70	2.55	7.42	41.6	228	89.3	134
W12×40	57.0	142	214	89.9	135	3.66	5.54	6.85	21.1	307	70.2	105
W10×45	54.9	137	206	85.8	129	2.59	3.89	7.10	26.9	248	70.7	106
W14×34	54.6	136	205	84.9	128	5.01	7.55	5.40	15.6	340	79.8	120
W16×31	54.0	135	203	82.4	124	6.86	10.3	4.13	11.8	375	87.5	131
W12×35	51.2	128	192	79.6	120	4.34	6.45	5.44	16.6	285	75.0	113
W8×48	49.0	122	184	75.4	113	1.67	2.55	7.35	35.2	184	68.0	102

Analysis Example - HW5

Q10-Q14

select W18 X 35 \rightarrow $W_t = 35 \text{ lb/ft}$

Q1

Q10 $W_{DL} = W_{DL}^* + W_t = 266 + 35 = 301 \text{ PLF}$

Q2

Q11 $W_u = 1.2 W_{DL} + 1.6 W_{LL} = 1.2 \times 301 + 1.6 \times 1260 = 2377.2 \text{ PLF}$
 $= 2.3772 \text{ KLF}$

Span A=27 FT

Q12 $M_u = \frac{W_u \cdot L^2}{8} = \frac{2.3772 (27)^2}{8} = 216.622 \text{ K-FT}$

Transfer to inch

Q13 $M_u = 216.622 \times 12 = 2599.46 \text{ K-IN}$

Q14 $\phi M_n = 0.9 (F_y \times Z_x) = 0.9 (50 \times 66.5) = 2992.5 \text{ K-IN}$

Q9