

# Arch324

# STRUCTURES II

Winter 2026  
Recitation

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# Recitation Guidelines

## Homework Problem

## Lab

- Please complete the lab sheet during recitation and hand it in before leaving.
- Try to attend all sessions. Unexcused absences will **affect your grade** starting from the second missed class.

# Analysis Example - HW6

## 6. Steel Column Analysis

For the given axially loaded steel W-section, determine the maximum floor live load capacity,  $P_{LL}$ . Assume the column is pinned top and bottom:  $K = 1.0$ , and there is no intermediate bracing. Use AISC-LRFD steel equations to determine  $\phi P_n$  and the load.  $E = 29000 \text{ ksi}$ .

DATASET: 1

-2-

-3-

W-section

W8X31

$F_y$

36 KSI

Span A

32 FT

Span B

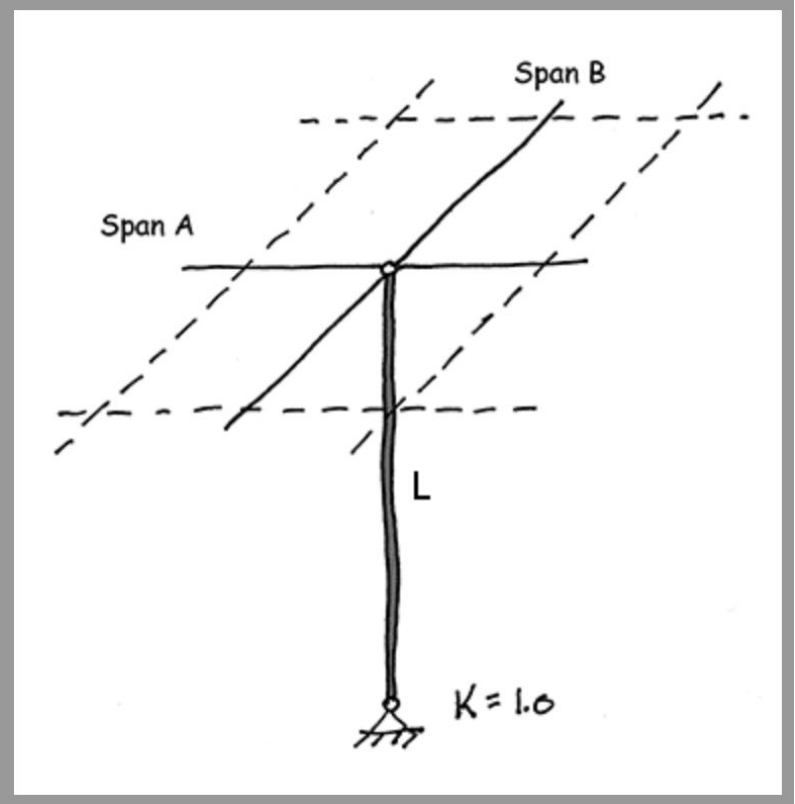
30 FT

Height L

17 FT

Floor Dead Load

39 PSF



# Analysis Example - HW6

9 Questions

#	<u>Question</u>	<u>Your Response</u>
1	Total unfactored floor dead load on the column	<input type="text"/> KIPS
2	Controlling slenderness ratio	<input type="text"/>
3	Transition slenderness value, $4.71(E/F_y)^{.5}$	<input type="text"/>
4	Euler stress, $F_e$	<input type="text"/> KSI
5	Critical stress, $F_{cr}$	<input type="text"/> KSI
6	Nominal strength, $P_n$	<input type="text"/> KIPS
7	Factored nominal strength, $\phi P_n$	<input type="text"/> KIPS
8	UN-factored live load on column (actual total LL)	<input type="text"/> KIPS
9	Actual unfactored floor live load	<input type="text"/> PSF

# Answer HW6

9 Questions

#	<u>Question</u>	<u>Your Response</u>	<u>Correct Answer</u>
1	Total unfactored floor dead load on the column	37.44 KIPS	37.44 KIPS
2	Controlling slenderness ratio	100.99	100.990099
3	Transition slenderness value, $4.71(E/F_y)^{.5}$	133.68	133.680683
4	Euler stress, $F_e$	28.03 KSI	28.06339101 KSI
5	Critical stress, $F_{cr}$	21.03 KSI	21.04363936 KSI
6	Nominal strength, $P_n$	192 KIPS	192.1284274 KIPS
7	Factored nominal strength, $\phi P_n$	172.8 KIPS	172.9155846 KIPS
8	UN-factored live load on column (actual total LL)	79.92 KIPS	79.9922404 KIPS
9	Actual unfactored floor live load	83.25 PSF	83.32525041 PSF

# Analysis Example - HW6

Tributary Area: Span A×Span B=32×30=960 FT<sup>2</sup>

Q1

Floor DL → 39×960=37440    37440/1000=37.44 KIPS    Q1

**Table 1-1 (continued)  
W-Shapes  
Dimensions**

Shape	Area, A in. <sup>2</sup>	Depth, d in.	Web				Flange				Distance				
			Thickness, tw in.	tw 2	Width, bf in.	Thickness, tf in.	k		k1	T	Work- able Gage in.				
							Kdes	Kdet							
W8×67	19.7	9.00	9	0.570	9/16	5/16	8.28	8 1/4	0.935	15/16	1.33	1 5/8	15 1/16	5 3/4	5 1/2
×58	17.1	8.75	8 3/4	0.510	1/2	1/4	8.22	8 1/4	0.810	13/16	1.20	1 1/2	7/8		
×48	14.1	8.50	8 1/2	0.400	3/8	3/16	8.11	8 1/8	0.685	1 1/16	1.08	1 3/8	13/16		
×40	11.7	8.25	8 1/4	0.360	3/8	3/16	8.07	8 1/8	0.560	9/16	0.954	1 1/4	13/16		
×35	10.3	8.12	8 1/8	0.310	5/16	3/16	8.02	8	0.495	1/2	0.889	1 3/16	13/16		
×31 <sup>f</sup>	9.13	8.00	8	0.285	5/16	3/16	8.00	8	0.435	7/16	0.829	1 1/8	3/4		

**Table 1-1 (continued)  
W-Shapes  
Properties**

W8-W4

Nom- inal Wt.	Compact Section Criteria		Axis X-X				Axis Y-Y				rtb	ho	Torsional Properties	
	bf 2tf	h tw	I in. <sup>4</sup>	S in. <sup>3</sup>	r in.	Z in. <sup>3</sup>	I in. <sup>4</sup>	S in. <sup>3</sup>	r in.	Z in. <sup>3</sup>			J in. <sup>4</sup>	Cw in. <sup>6</sup>
67	4.43	11.1	272	60.4	3.72	70.1	88.6	21.4	2.12	32.7	2.43	8.07	5.05	1440
58	5.07	12.4	228	52.0	3.65	59.8	75.1	18.3	2.10	27.9	2.39	7.94	3.33	1180
48	5.92	15.9	184	43.2	3.61	49.0	60.9	15.0	2.08	22.9	2.35	7.82	1.96	931
40	7.21	17.6	146	35.5	3.53	39.8	49.1	12.2	2.04	18.5	2.31	7.69	1.12	726
35	8.10	20.5	127	31.2	3.51	34.7	42.6	10.6	2.03	16.1	2.28	7.63	0.769	619
31	9.19	22.3	110	27.5	3.47	30.4	37.1	9.27	2.02	14.1	2.26	7.57	0.536	530

From Table 1-1: W8×31    rx=3.47 in    ry=2.02 in    A=9.13 in<sup>2</sup>

# Analysis Example - HW6

Q2-Q7

Euler equation:

$$F_e = \frac{\pi^2 E}{\left(\frac{KL}{r}\right)^2}$$

Short & Intermediate Columns:

$$F_{cr} = \left[0.658^{\frac{F_y}{F_e}}\right] F_y$$

$$P_n = F_{cr} A_g$$

$$\phi_c P_n = \phi_c F_{cr} A_g$$

Given:  $k=1$ , Height  $L=17$  FT

Transfer to inch

$$\lambda_x = \frac{KL}{r_x} = \frac{1 \times 17 \times 12}{3.47} = 58.79 < 200$$

Q2  $\lambda_y = \frac{KL}{r_y} = \frac{1 \times 17 \times 12}{2.02} = 100.99 < 200$  (✓)

Maximum

Q3  $4.71 \sqrt{\frac{E}{F_y}} = 4.71 \sqrt{\frac{29000}{36}} = 133.68$

Q4  $F_e = \frac{\pi^2 E}{\left(\frac{KL}{r}\right)^2} = \frac{(3.14)^2 \cdot 29000}{(100.99)^2} = 28.03$  KSI

Q5  $F_{cr} = \left[0.658^{\frac{F_y}{F_e}}\right] F_y = \left[0.658^{\frac{36}{28.03}}\right] \cdot 36 = 21.03$  KSI

A area from Table 1-1

Q6  $P_n = F_{cr} \cdot A = 21.03 \times 9.13 = 192.0039$  KIPS

Q7  $\phi P_n = 0.9 \times 192.0039 = 172.80$  KIPS

# Analysis Example - HW6

Q8-Q9

Q7

$$P_u = 1.2 P_D + 1.6 P_L = 1.2 \times 37.44 + 1.6 P_L \leq \phi P_n = 172.8$$

Q8  $\rightarrow P_L = \frac{\phi P_n - 1.2 P_D}{1.6} = \frac{172.8 - 1.2 \times 37.44}{1.6} = 79.92 \text{ KIPS}$  Q1=PD

Q9  $\frac{P_L}{\text{Tributary Area}} = \frac{79.92 \times 1000}{960} = 83.25 \text{ PSF}$  Transfer to LB