

Arch 324

Structures II

Winter 2026 Recitation 004

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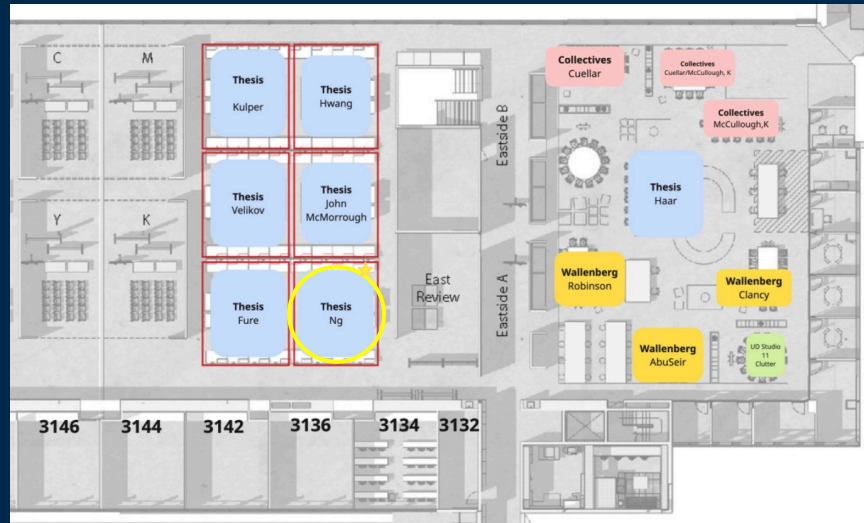
GSI Info :)

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Recitation 004

Welcome to session 3!















- Tower Heads up
- Quick Lecture Recap
- Homework #3 Wood Column Design
- Lab: Wood Columns

Tower!!

M MICHIGAN
Architecture

Structures
Project

Contact Schedule Lectures Recitation **Towers 1** Towers2 Problems

- [Testing Signup Sheet](#) 
- [Tower Project Brief 2026](#) 
- [Prelim Report Guidelines 2026](#) 
- [Final Report Guidelines 2026](#) 
- [Score Sheet 2026](#) 
- [Study of Tower Types](#) 
- [Example Reports](#) 
- [Dr. Frame Software \(download\)](#) 
- [Rhino to Dr. Frame converter](#) 
- [Dr. Frame Tutorials](#)   
- [STAAD example](#) 
- [Videos of Old Tower Tests](#) 

Lecture: Wood Column Design

Failure Mode - Strength

Short Columns – fail by crushing

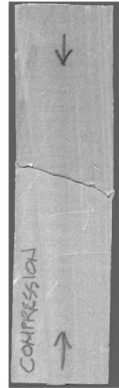
Analysis

$$f_c = \frac{P}{A} \leq F'_c$$

- f_c = Actual compressive stress
- A = Cross-sectional area of column (in²)
- P = Load on the column
- F'_c = Allowable compressive stress per codes

Design

$$A = \frac{P}{F'_c}$$



Failure Modes – Stability

Long Columns – fail by buckling

Traditional Euler

$$f_{cr} = \frac{\pi^2 E}{\left(\frac{KL}{r}\right)^2}$$

- E = Modulus of elasticity of the column material (psi)
- K = Stiffness (curvature mode) factor
- L = Column length between ends (inches)
- r = radius of gyration = $\sqrt{I/A}$ (inches)

NDS Equation

$$F_{cE} = \frac{0.822 E'_{min}}{\left(\frac{l_e}{d}\right)^2}$$

- E'_{min} = reduced E modulus (psi)
- $l_e = K_e l_u$ (inches)
- d (inches)
- $0.822 = \pi^2/12$



$$r = d/\sqrt{12}$$

Lecture: Wood Column Design

Capacity Analysis of Columns

Data:

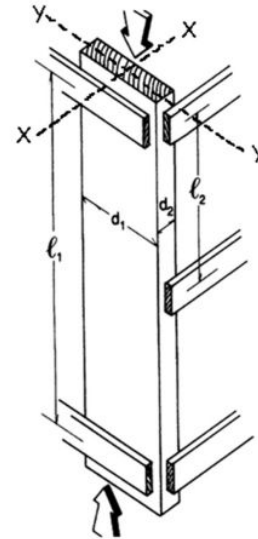
- Column – size, length
- Support conditions
- Material properties – F_c , E_{min}

Required:

- Maximum Load Capacity, P_{max}

1. Calculate slenderness ratio l_e/d
largest ratio governs. Must be < 50
2. Find adjustment factors
 $C_D C_M C_t C_F C_i$
3. Calculate C_p
4. Determine F'_c by multiplying the tabulated F_c
by all the above factors
5. Set actual stress = allowable, $f_c = F'_c$
6. Find the maximum allowable load

$$P_{max} = F'_c A$$



Lecture: Wood Column Design

Adjustment Factors

Table 4.3.1 Applicability of Adjustment Factors for Sawn Lumber

	ASD only	ASD and LRFD										LRFD only			
		Load Duration Factor	Wet Service Factor	Temperature Factor	Beam Stability Factor	Size Factor	Flat Use Factor	Incising Factor	Repetitive Member Factor	Column Stability Factor	Buckling Stiffness Factor	Bearing Area Factor	Format Conversion Factor	Resistance Factor	Time Effect Factor
		K_D											ϕ		
$F_b' = F_b$	x	C_D	C_M	C_t	C_L	C_F	C_{fu}	C_i	C_r	-	-	-	2.54	0.85	λ
$F_t' = F_t$	x	C_D	C_M	C_t	-	C_F	-	C_i	-	-	-	-	2.70	0.80	λ
$F_v' = F_v$	x	C_D	C_M	C_t	-	-	-	C_i	-	-	-	-	2.88	0.75	λ
$F_c' = F_c$	x	C_D	C_M	C_t	-	C_F	-	C_i	-	C_p	-	-	2.40	0.90	λ
$F_{cL}' = F_{cL}$	x	-	C_M	C_t	-	-	-	C_i	-	-	-	C_b	1.67	0.90	-
$E' = E$	x	-	C_M	C_t	-	-	-	C_i	-	-	-	-	-	-	-
$E_{min}' = E_{min}$	x	-	C_M	C_t	-	-	-	C_i	-	-	C_T	-	1.76	0.85	-

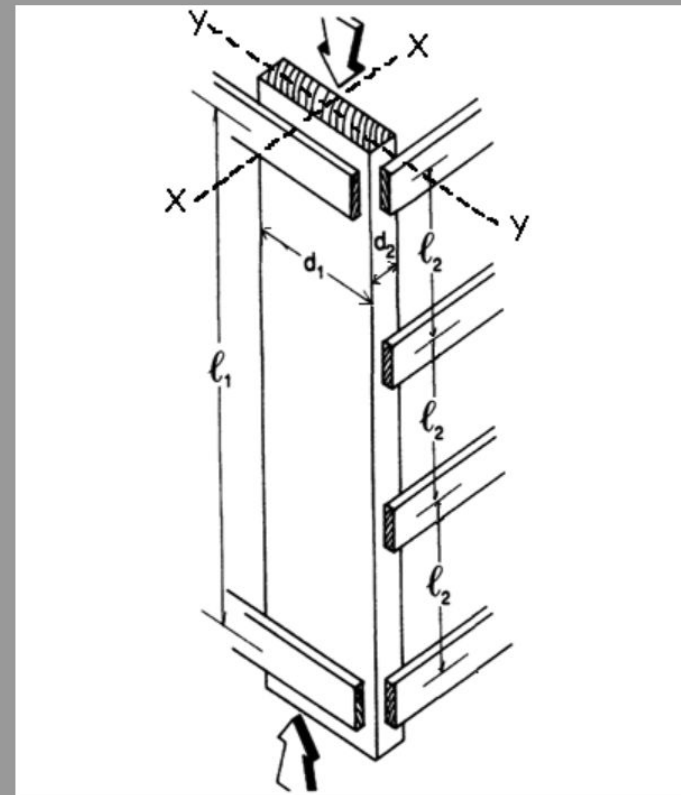
HW #3: Wood Column Design

3. Wood Column Analysis

For the given dimensioned lumber column with 1/3 point weak axis bracing," determine the maximum load capacity of the given load type. Moisture Content = 15%. $C_t = C_i = 1.0$. Assume pinned end conditions ($K=1$).

DATASET: 1 -2- -3-

Wood Species	WESTERN CEDARS
Wood Grade	No.1
Strong Axis Length, L_1	8 FT
Weak Axis Length, L_2	2.666666667 FT
Narrow Width, d_2	4 IN
Wide Width, d_1	10 IN
LoadType	Wind Load



HW #3: Wood Column Design

Table 4A (Cont.) Reference Design Values for Visually Graded Dimension Lumber (2" - 4" thick)^{1,2,3}

(All species except Southern Pine—see Table 4B) (Tabulated design values are for normal load duration and dry service conditions. See NDS 4.3 for a comprehensive description of design value adjustment factors.)

USE WITH TABLE 4A ADJUSTMENT FACTORS

Species and commercial grade	Size classification	Design values in pounds per square inch (psi)							Specific Gravity ⁴ G	Grading Rules Agency
		Bending F _b	Tension parallel to grain F _t	Shear parallel to grain F _v	Compression perpendicular to grain F _{c⊥}	Compression parallel to grain F _c	Modulus of Elasticity			
							E	E _{min}		
WESTERN CEDARS										
Select Structural		1,000	600	155	425	1,000	1,100,000	400,000		
No. 1	2" & wider	725	425	155	425	825	1,000,000	370,000	0.36	WCLIB WWPA
No. 2		700	425	155	425	650	1,000,000	370,000		
No. 3		400	250	155	425	375	900,000	330,000		
Stud	2" & wider	550	325	155	425	400	900,000	330,000		
Construction		800	475	155	425	850	900,000	330,000		
Standard	2" - 4" wide	450	275	155	425	650	800,000	290,000		
Utility		225	125	155	425	425	800,000	290,000		

Q1

Q2

HW #3: Wood Column Design

Table 2.3.2 Frequently Used Load Duration Factors, C_D^1

Load Duration	C_D	Typical Design Loads
Permanent	0.9	Dead Load
Ten years	1.0	Occupancy Live Load
Two months	1.15	Snow Load
Seven days	1.25	Construction Load
Ten minutes	1.6	Wind/Earthquake Load
Impact ²	2.0	Impact Load

Q3

LoadType

Wind Load

HW #3: Wood Column Design

Size Factor, C_F

Tabulated bending, tension, and compression parallel to grain design values for dimension lumber 2" to 4" thick shall be multiplied by the following size factors:

Size Factors, C_F

Grades	Width (depth)	F_b		F_t	F_c
		Thickness (breadth)			
		2" & 3"	4"		
Select Structural, No.1 & Btr, No.1, No.2, No.3	2", 3", & 4"	1.5	1.5	1.5	1.15
	5"	1.4	1.4	1.4	1.1
	6"	1.3	1.3	1.3	1.1
	8"	1.2	1.3	1.2	1.05
	10"	1.1	1.2	1.1	1.0
	12"	1.0	1.1	1.0	1.0
	14" & wider	0.9	1.0	0.9	0.9
Stud	2", 3", & 4"	1.1	1.1	1.1	1.05
	5" & 6"	1.0	1.0	1.0	1.0
	8" & wider	Use No.3 Grade tabulated design values and size factors			
Construction, Standard	2", 3", & 4"	1.0	1.0	1.0	1.0
Utility	4"	1.0	1.0	1.0	1.0
	2" & 3"	0.4	—	0.4	0.6

Q4

HW #3: Wood Column Design

For the given dimensioned lumber column with 1/3 point weak axis bracing", determine the maximum load capacity of the given load type. Moisture Content = 15%. $C_t = C_i = 1.0$. Assume pinned end conditions ($K=1$).

$$C_t = 1.0$$
$$C_i = 1.0$$

$$C_M = 1.0$$

Wet Service Factor, C_M

When dimension lumber is used where moisture content will exceed 19% for an extended time period, design values shall be multiplied by the appropriate wet service factors from the following table:

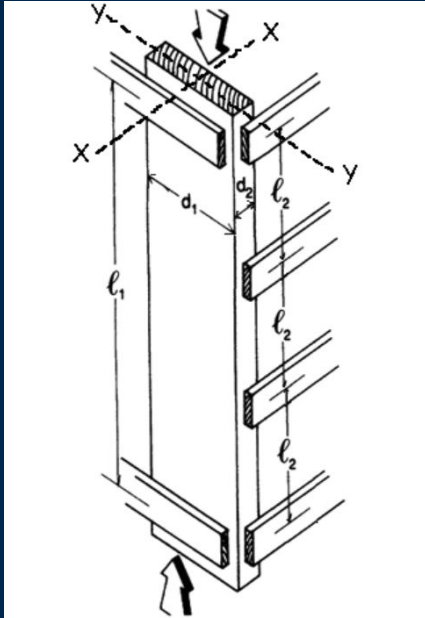
Wet Service Factors, C_M

F_b	F_t	F_v	F_{cL}	F_c	E and E_{min}
0.85*	1.0	0.97	0.67	0.8**	0.9

* when $(F_b)(C_F) \leq 1,150$ psi, $C_M = 1.0$

** when $(F_c)(C_F) \leq 750$ psi, $C_M = 1.0$

HW #3: Wood Column Design



$$9. F_{cE} = \frac{0.822 (370,000)^{\#5}}{(10.378)^2 \#8} = \boxed{2,823.88} \text{ PSI}$$

Answer to #9

$$10. F_c^* = C_D \cdot C_M \cdot C_t \cdot C_F \cdot C_i \cdot F_c$$

(1.6) (1) (1) (1) (1) (825)
 #3 wet service #4 #1

$$= \boxed{1,320} \text{ PSI} \leftarrow \text{Answer to #10}$$

11. $c = 0.8$ for sawn lumber

$$12. C_p = \frac{1 + \left(\frac{2,823.88}{1,320}\right)}{2(0.8)} - \sqrt{\left[\frac{1 + \left(\frac{2,823.88}{1,320}\right)}{2(0.8)}\right]^2 - \frac{\left(\frac{2,823.88}{1,320}\right)}{0.8}}$$

$$= 1.9621 - \sqrt{(1.9621)^2 - 2.6741}$$

$$= \boxed{0.89} \leftarrow \text{Answer to #11}$$

HW #3: Wood Column Design

Table 1B Section Properties of S

Nominal Size b x d	Standard Dressed Size (S4S) b x d in. x in.	Area of Section A in. ²	X-X AX	
			Section Modulus S _{xx} in. ³	Mo
4 x 4	3-1/2 x 3-1/2	12.25	7.15	12
4 x 5	3-1/2 x 4-1/2	15.75	11.81	26
4 x 6	3-1/2 x 5-1/2	19.25	17.65	48
4 x 8	3-1/2 x 7-1/4	25.38	30.66	11
4 x 10	3-1/2 x 9-1/4	32.38	49.91	23
4 x 12	3-1/2 x 11-1/4	39.38	73.83	41
4 x 14	3-1/2 x 13-1/4	46.38	102.41	67
4 x 16	3-1/2 x 15-1/4	53.38	135.66	10

Q14

#3. $F'_c = C_p \cdot C_m \cdot C_t \cdot C_F \cdot C_i \cdot C_p \cdot F_c$
 $(1.6) \cdot (1) \cdot (1) \cdot (1) \cdot (1) \cdot (0.89) \cdot (825)$
 #3 net size #4 #11 #1
 $= 1,174.8 \text{ psi} \leftarrow \text{Answer to \#13}$

#15. $P_{max} = F'_c \cdot A = 1174.8 (32.38)$
 $= 38,040.02 \text{ lbs}$
 Answer to #15

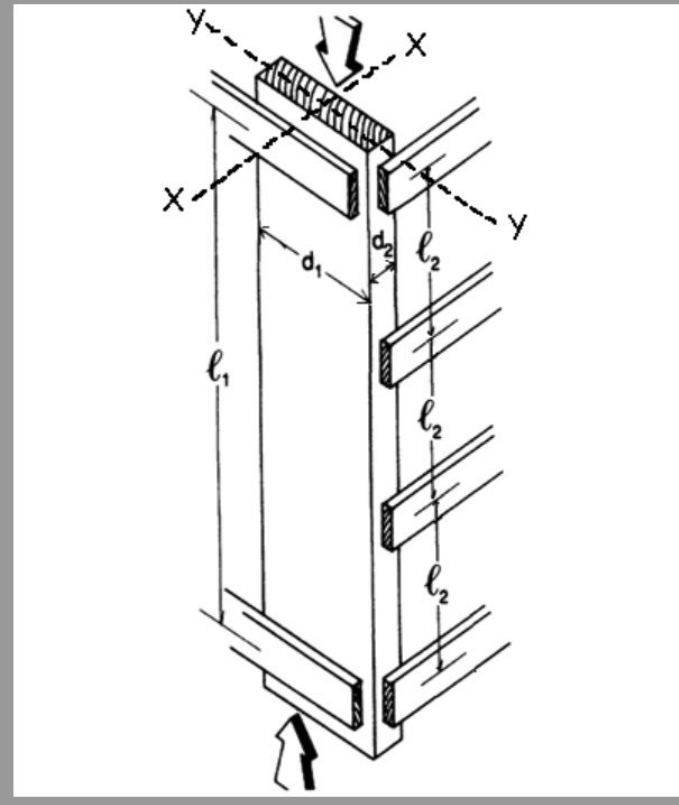
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LAB!

